Ascarite II Performance as a Carbon Dioxide Scrubber: Use with the Fumiscope Fumigant Monitoring Instrument.

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Background

During the course of Methyl Bromide (MeBr) fumigation, certain commodities (green wood, produce) evolve varying and significant amounts of Carbon dioxide (CO_2). This CO_2 registers as MeBr on fumigant monitors that use non-discriminatory thermal conductivity technology. The product Ascarite II (Sodium hydroxide based) can remove CO_2 from the sample stream. However, its longevity and performance in conjunction with the Fumiscope and at several CO_2 concentrations has not been verified or well-documented.

Brief Project Outline

The initial objectives were to 1.) Document and quantify possible blow-by of CO2 through Ascarite. By that, we mean the amount of CO_2 that may pass the Ascarite tube without being scrubbed. 2.) Determine how long and how efficiently tubes of Ascarite II will perform to our specifications when CO_2 of concentrations from 0.5 up to 5% are present under conditions of use during typical fumigation monitoring. These experiments were conducted at the USDA, APHIS, CPHST, NRMAL facility in Gulfport, MS. Project supported under Project 94181-C9Q51.

Initial Calibration Tests.

The Qubit S-157 CO_2 Analyzer (the Qubit) was calibrated at 0-2000 ppm CO2 as follows. Clean cylinder air was passed through a Drierite tube (#26930, 10-20 mesh), then through a polycarbonate Ascarite II tube (made from an empty Drierite 26930 tube) to clean all CO_2. Using factory calibration, this produced a reading of 0 ppm CO_2 on the Qubit. The flow was adjusted to an index of 75 on the Gilmont indexed flow gauge (the Gauge). Tables from Gilmont indicated that this would supply about 475 ml/min air flow. T he Qubit was then calibrated at 0 ppm CO_2. Then, the Ascarite tube was removed and the Qubit was calibrated at 2000 ppm CO_2 by preparing a 3-L gas bag with 2000 ppm CO_2, and then allowing the gas to flow through the Qubit. Lastly, air flow was produced by connecting an Air Cadet vacuum pump in-line, after the Qubit. The equipment set-up for calibration is shown in Figure 1. below. Following this, a calibration check was performed by passing 2000 ppm CO2, applying the Ascarite tube after about 2.5 minutes, and then removing the Ascarite tube after about 6.5 minutes. The resultant evidence of accurate calibration is presented below in Figure 2.

Figure 1. Set-up of the Qubit CO2 for calibration, with (r-l) sample supply bag, Drierite tube, Ascarite (in Drierite tube), Gilmont gauge, Qubit S-157 CO_2 analyzer, and Air Cadet vacuum source.

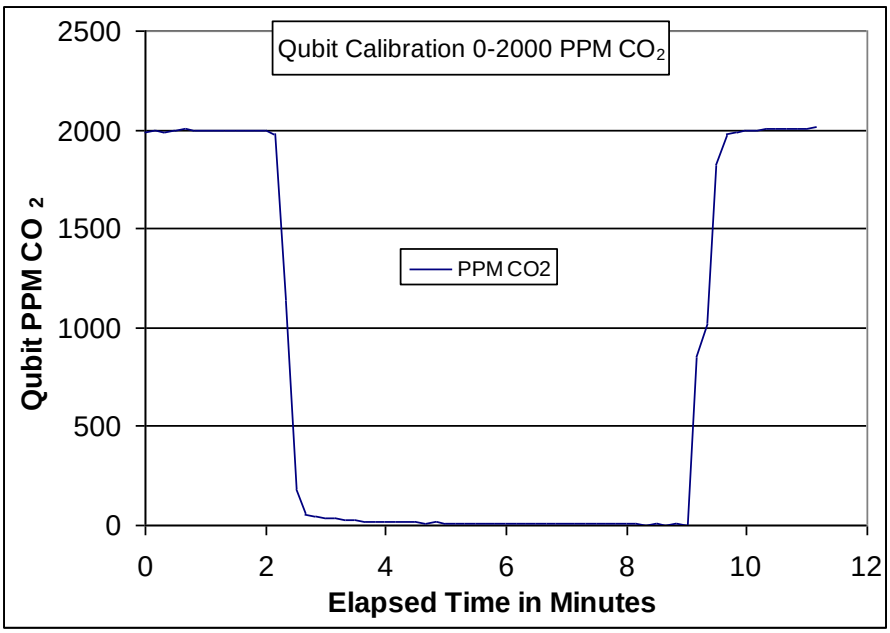


Figure 2. Verification of zero and 2000 ppm CO_2 span of the Qubit analyzer.

Initial tests for blow-by of CO_2.

A Fumiscope tube was prepared with 10 g 20-30 mesh Ascarite. A supply of 5% CO_2 in a 100-L gas bag was connected so as to pass through a Drierite tube, the Ascarite, the flow gauge, and then the Qubit. PPM CO_2 was logged every 10 seconds, and the and air flow was recorded every 5 minutes or when a significant change was noted. The experiment was continued until CO_2 was detected passing through the Ascarite. The result is shown below in Figure 3.

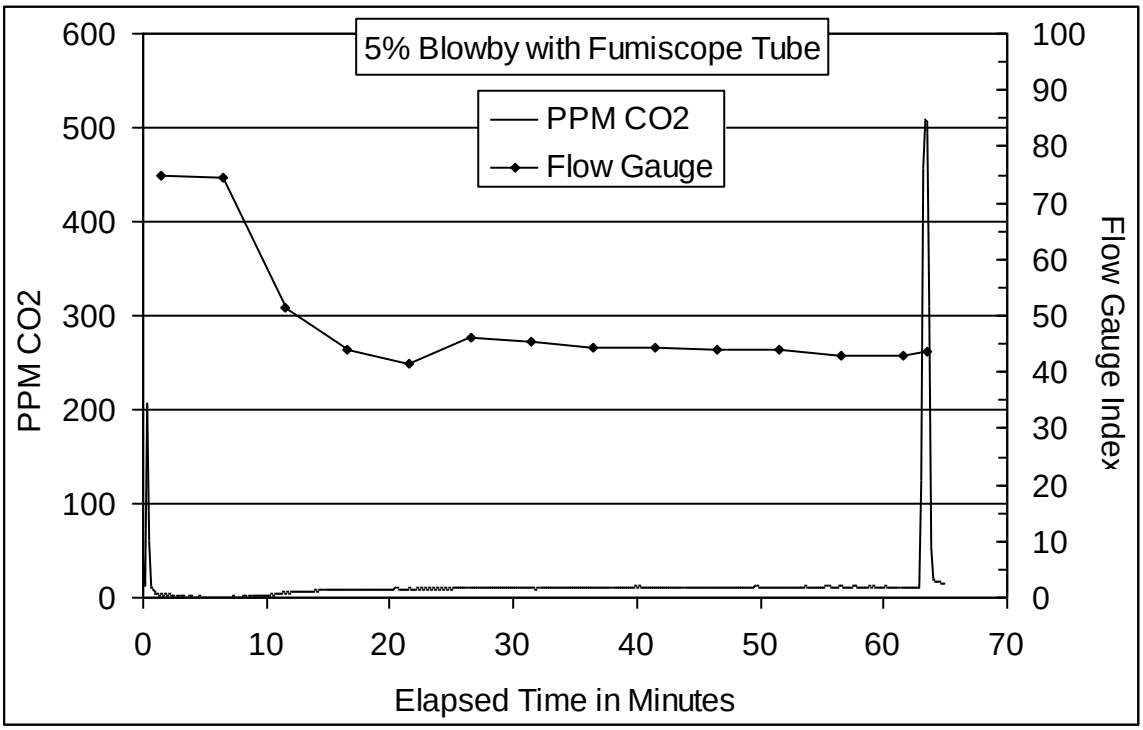


Figure 3.

After connection of the Ascarite tube, CO_2 remained at trace levels (ca. 10 ppm). After about 63.5 minutes, an attempt was made to bring air flow back to about 75 on the gauge. This was not successful. It was apparent that, although we were able to scrub CO_2 from the sample stream, this was only done with a decrease in air flow caused by plugging of the Ascarite and therefore much greater vacuum needed to pull the sample through the tube. The condition of the Ascarite tube is shown in Figure 4.

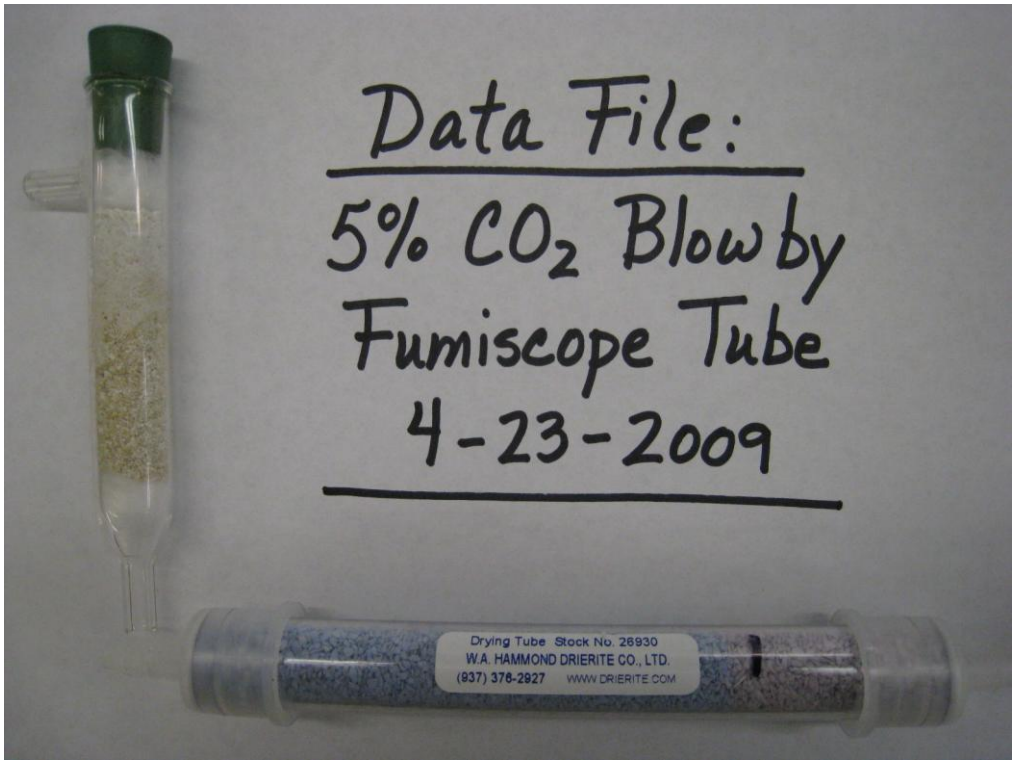


Figure 4. Glass Ascarite tube after tube became plugged.

With sufficient vacuum applied, we could continue to force the scrubbing of 5% CO_2. Only a small proportion of the Ascarite tube was consumed, before complete stoppage required ending the test.

An alternative Ascarite tube arrangement was tested. A piece of Tygon tube (10 mm OD, 6 mm ID) was fitted made to hold 10.0 g Ascarite. The flexible tube allowed us to manipulate the tube to break up plugging, thus allowing air flow and CO_2 to run to completion, thus consuming the entire tube. It was our theory that as long as air flowed, the Ascarite would scrub CO_2 without significant blow-by. The system was run continually, and each time air flow appeared to decrease, the tube was flexed, thus breaking up any stoppage and allowing the reaction front to move through the tube. The result is shown in Figure 5, below. As long as a small amount of Ascarite is available for the scrubbing reaction, the procedure is effective. However, this is not a practical procedure. But, it does clearly show blow-by is not an issue as long as air flow can be continued. This raises questions of pump performance, which will be discussed later.

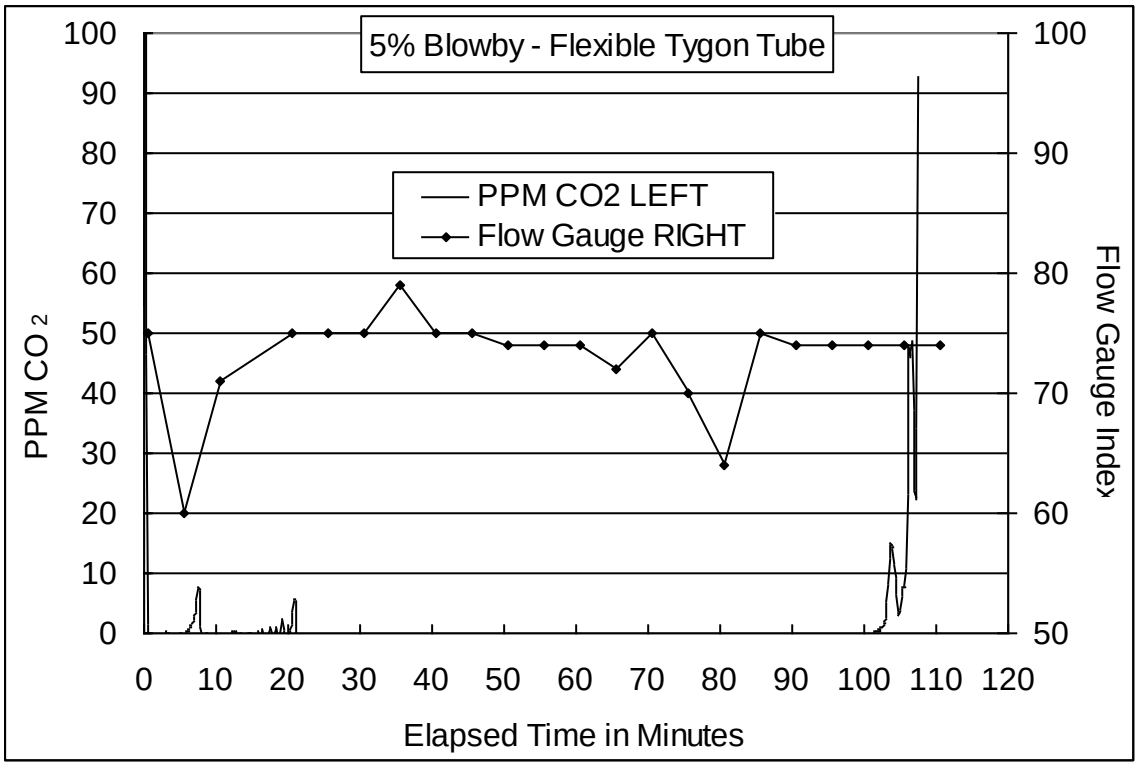


Figure 5. Performance of 10 g Ascarite in a flexible 6 mm ID Tygon tube with a constant supply of 5% CO_2.

By breaking up flow stoppage due to the Ascarite/CO_2 reaction front, we were able to continue to scrub CO_2 until the tube was almost completely used up. Evidence of this is shown in Figure 6. The failure of an Ascarite tube to function over time with high CO_2 is the result of plugging, not blow-by.

Tests with Variable CO_2 Concentrations and 20-30 Mesh Ascarite II.

The following tests were conducted using the Fumiscope, a standard glass Ascarite tube filled with 10 g of 20-30 mesh Ascarite II. Air movement was provided by the Fumiscope pump, and measured using the integral flow gauge. In addition, a precision digital manometer was placed in-line with a T connector to monitor the pressure drop (vacuum) created when the system needed to overcome tube plugging. Concentrations of 0.5, 1.0, 2.0, 3.0, 4.0, and 5.0 % CO_2 were used. The experimental set-up is shown below in Figure 7. The order of flow was: gas bag, Drierite, Ascarite, T-offset manometer, Fumiscope. Fumiscope flow was adjusted back to 1.0 SCFH if sample flow dropped to less than 0.9 SCFH (ca. 472 ml/min). The Fumiscope was zeroed with cylinder air, and re-zeroed after the first minute, to compensate for any pressure effects on the zero point.

The results of all tests are presented graphically, showing Fumiscope flow rate, g/m3, and vacuum in mm Hg. Tests were discontinued after Ascarite was used up, or g/m3 or pressure readings indicated plugging was complete.

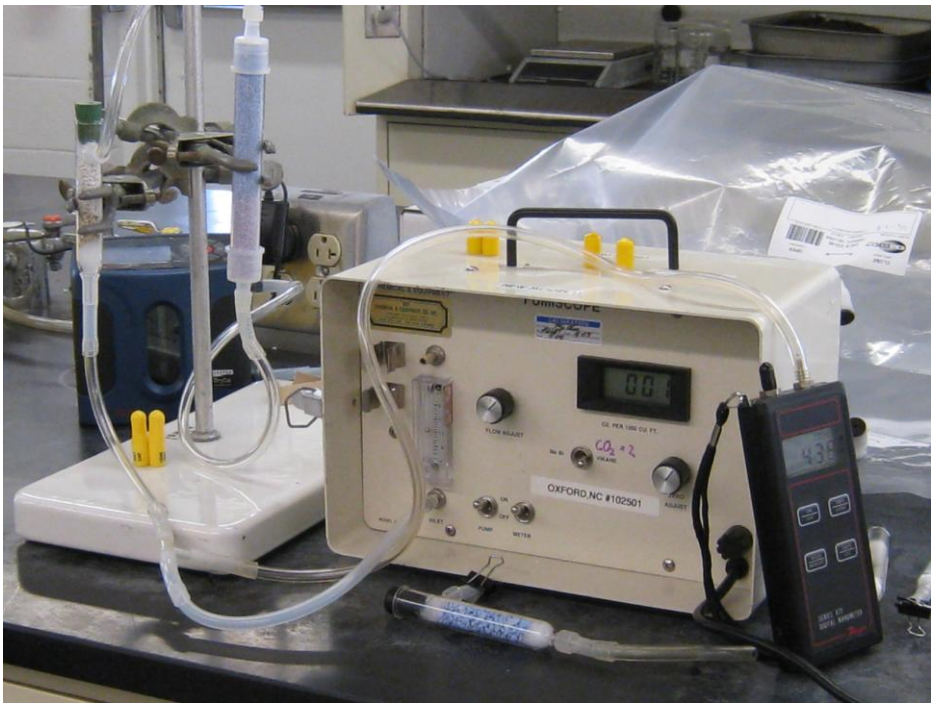


Figure 7. Experimental set-up of 100-L gas-bag CO_2 supply, Fumiscope with digital manometer, Drierite tube, and glass Ascarite tube.

Figure 8. Tests with 0.5% CO_2, 20-30 mesh Ascarite II. The tube was practically used up after 3.5 hours, and vacuum draw remained low, indicting good sample air flow. However, Fumiscope flow was adverse at about 175 minutes.

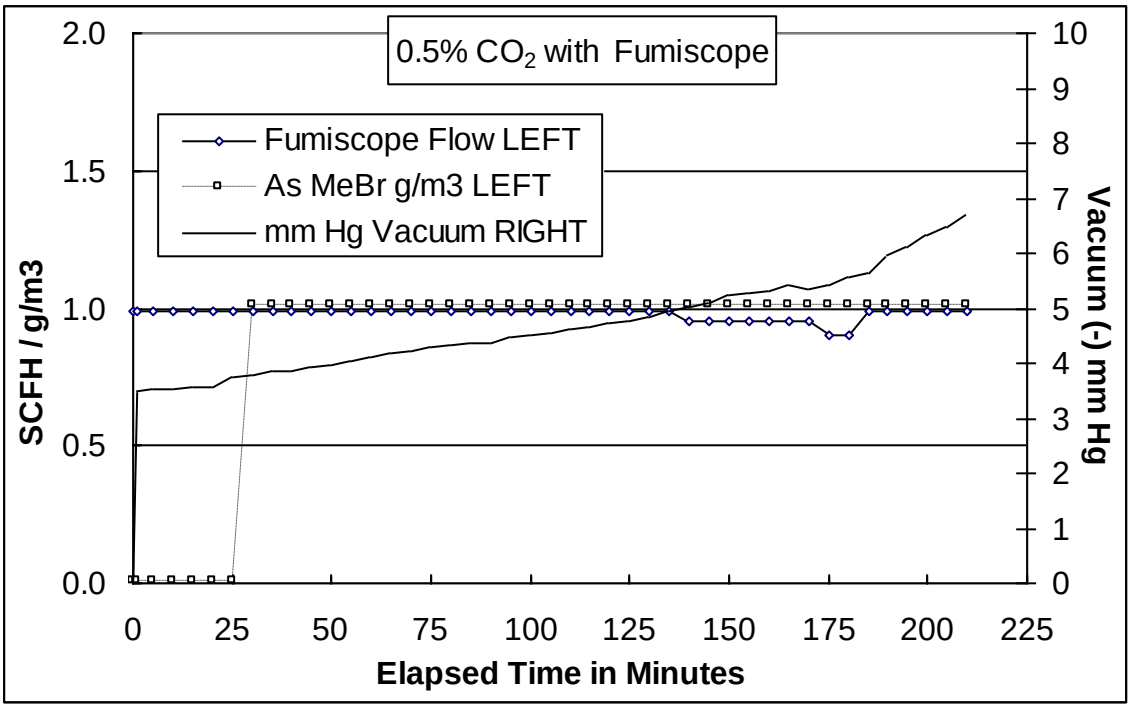


Figure 9. Tests with 1.0% CO_2 and 20-30 mesh Ascarite II. A vacuum increase coincided with increase in Fumiscope g/m^3 as MeBr and after flow could no longer be kept at 1.0 SCFH due to pump overload. Failure estimated to be after about 95minutes.

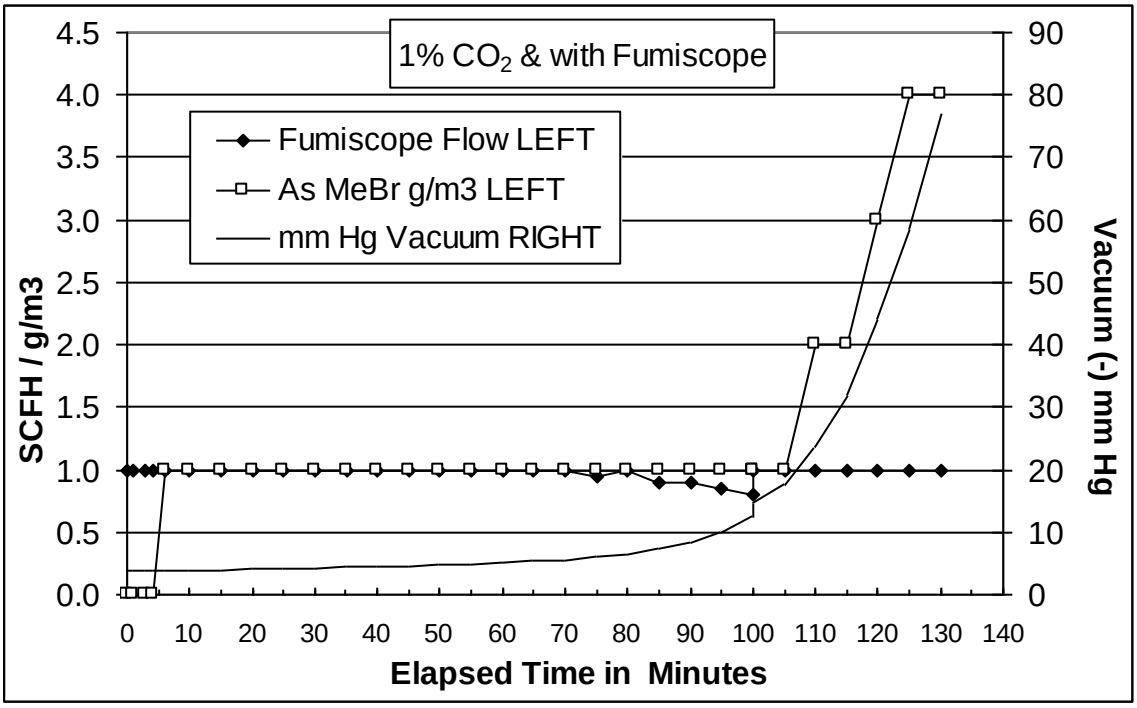


Figure 10. Tests with 2% CO_2 and 20-30 mesh Ascarite II. Increased vacuum and g/m^3 as MeBr coincidentally increased to undesirable levels after about 10 minutes.

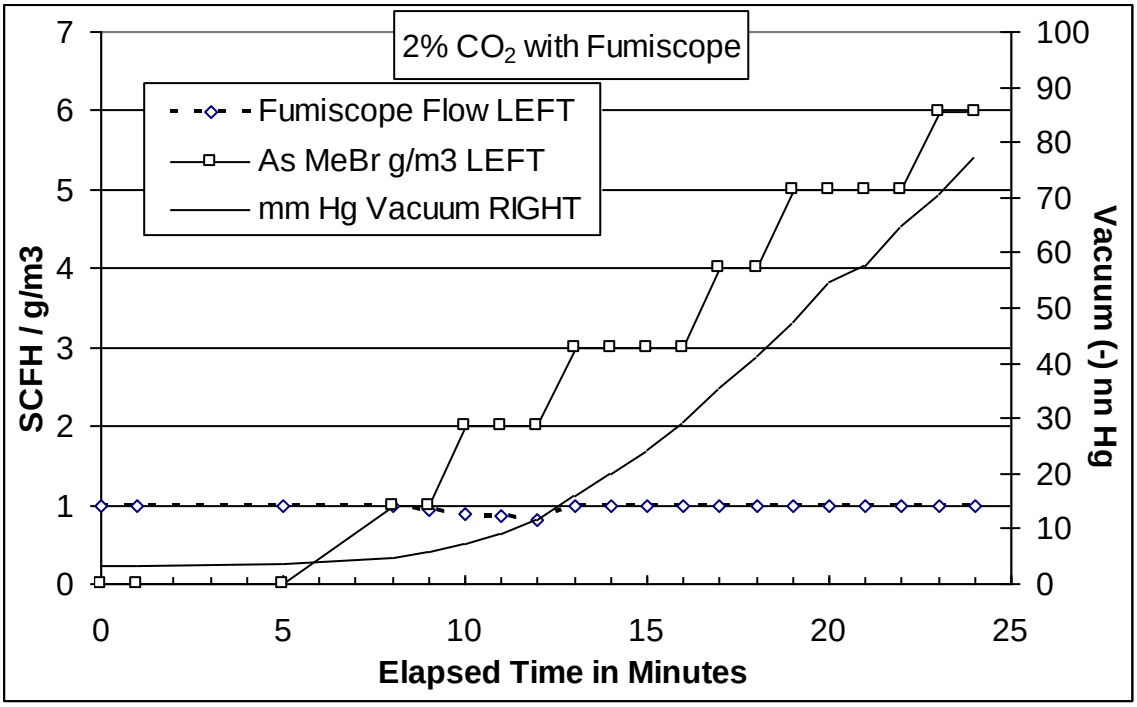


Figure 11. Tests with 3% CO_2 and 20-30 mesh Ascarite II. Increased vacuum and Fumiscope readings as g/m^3 MeBr began after about six minutes.

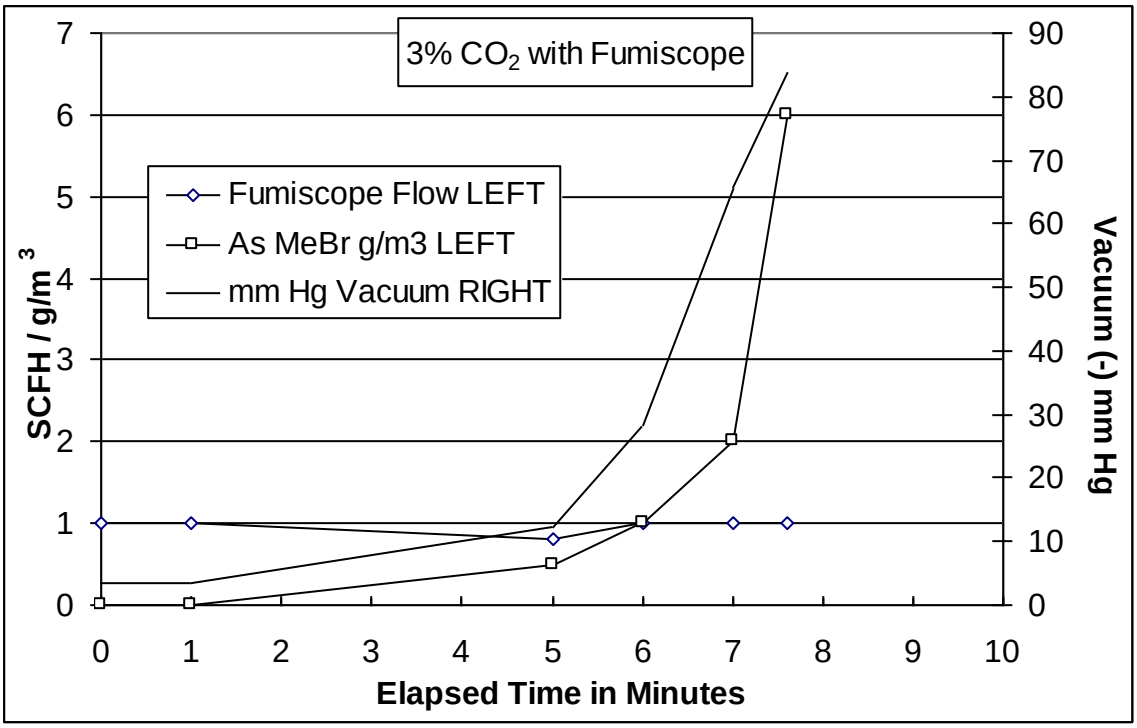


Figure 12. Tests with 4% CO_2 and 20-30 mesh Ascarite II. Failure due to increased vacuum, Fumiscope pump overload and increase in g/m3 as MeBr indication after about three minutes.

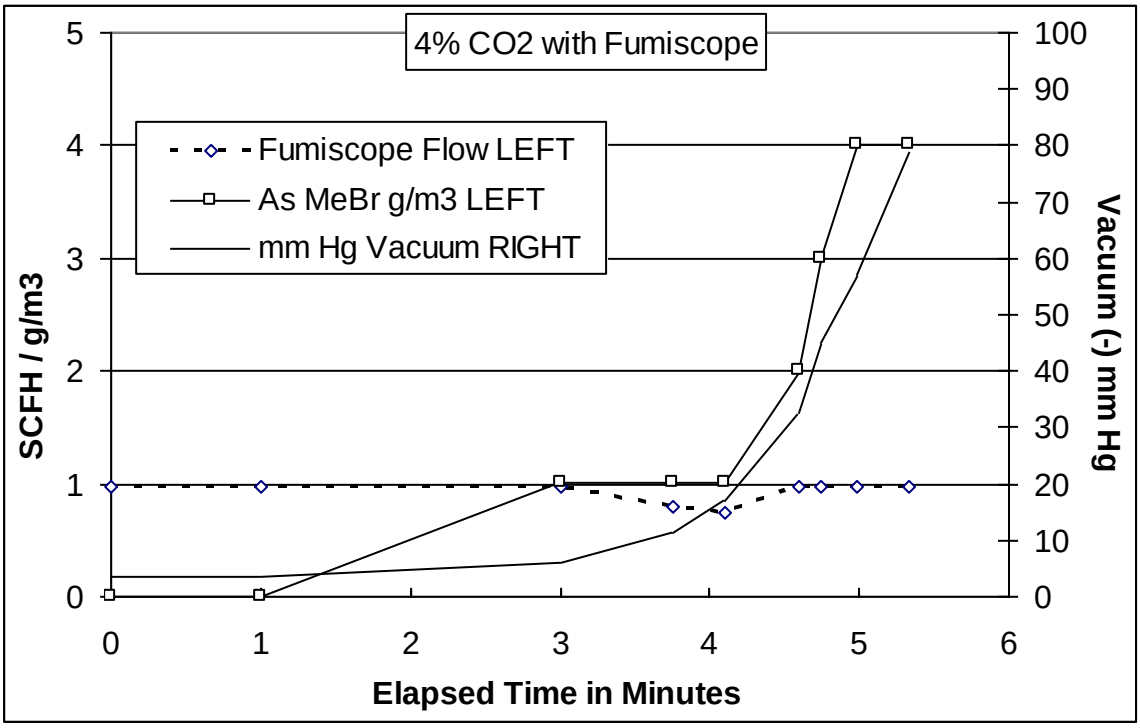
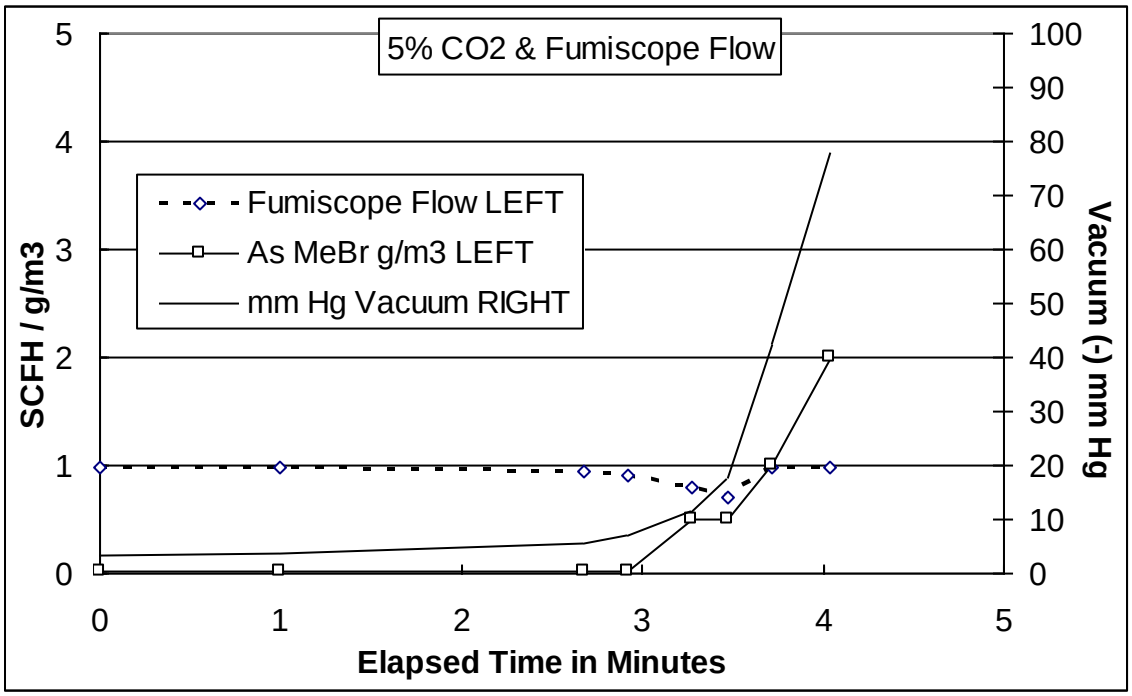


Figure 13. Tests with 5% CO_2 and 20-30 mesh Ascarite II. Failure due to increase vacuum, Fumiscope pump overload and increase in g/m3 as MeBr occurred after less than three minutes.



Flow rate vs. Pressure with 5% CO2. A test to compare the increased vacuum draw and effect on the Fumiscope reading was performed by supplying 5% CO2 and then observing the reduction in air flow and corresponding changes in Fumiscope readings. For this test, the Defender 510 (the Defender) precision flow rate calibrator was placed in line. Data was recorded at each time the Fumiscope flow gauge dropped 0.1 SCFH, down to 0.3 SCFH. The result is shown below in Figure 14.

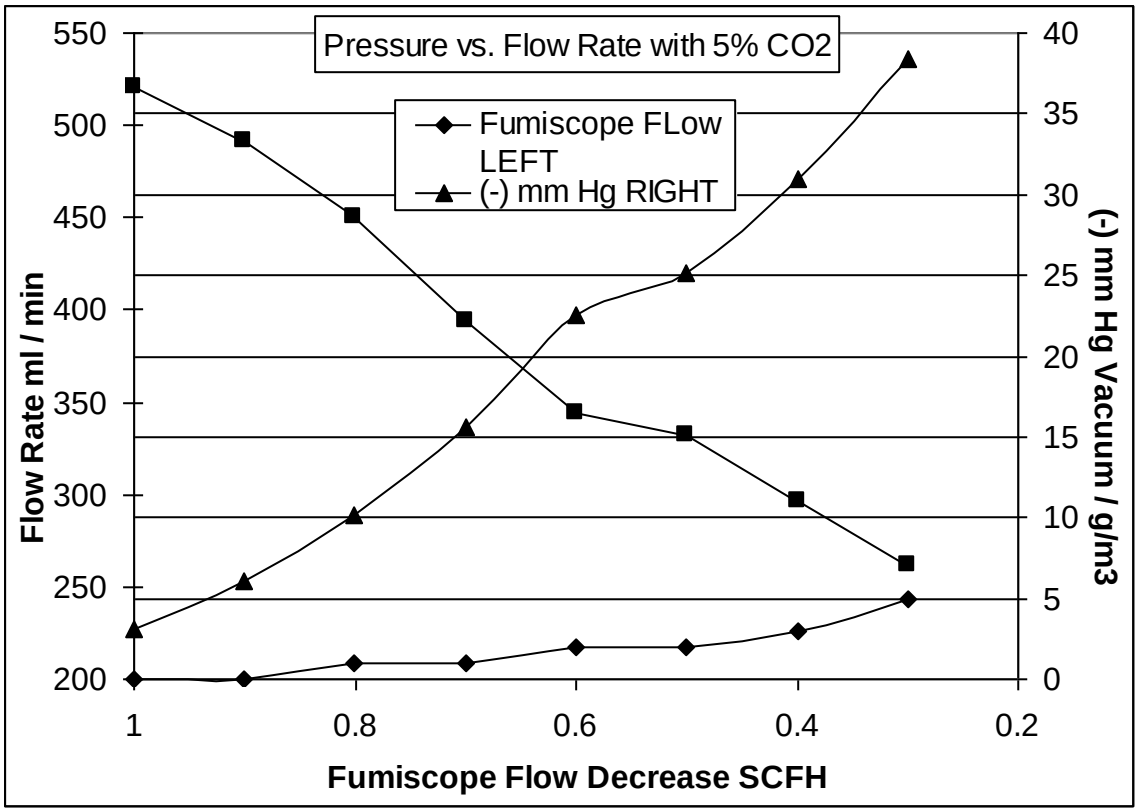


Figure 14. Relation of vacuum draw to flow rate and Fumiscope reading with constant supplied 5% CO_2.

From these data, it is clear that plugging of the Ascarite tube has a drastic effect on flow rates and the vacuum needed to draw a sample through the Fumiscope. The ability of the Fumiscope to maintain a 1.0 SCFH flow rate is compromised, and that even when flow can be adjusted to the point where the pump is at maximum, significant influence on the Fumiscope reading was observed.

The severity of the plugging issue with 20-30 mesh Ascarite II caused us to consider 8-20 mesh as a possible solution. With fine mesh Ascarite II, the reaction proceeds quickly and over a narrow reaction front, thus using only a small amount of the available material, and causing the system to fail in only a few minutes at all but the lowest concentrations of CO2. We conducted a blow-by test with 5% CO_2, the 8-20 mesh material (10.1 g in a Fumiscope tube), using the Qubit and a steady air flow rate of 74.5-75.0 on the Gilmont flow gauge. Results were recorded at 10 second intervals by the Qubit. The result is shown below in Figure 15.

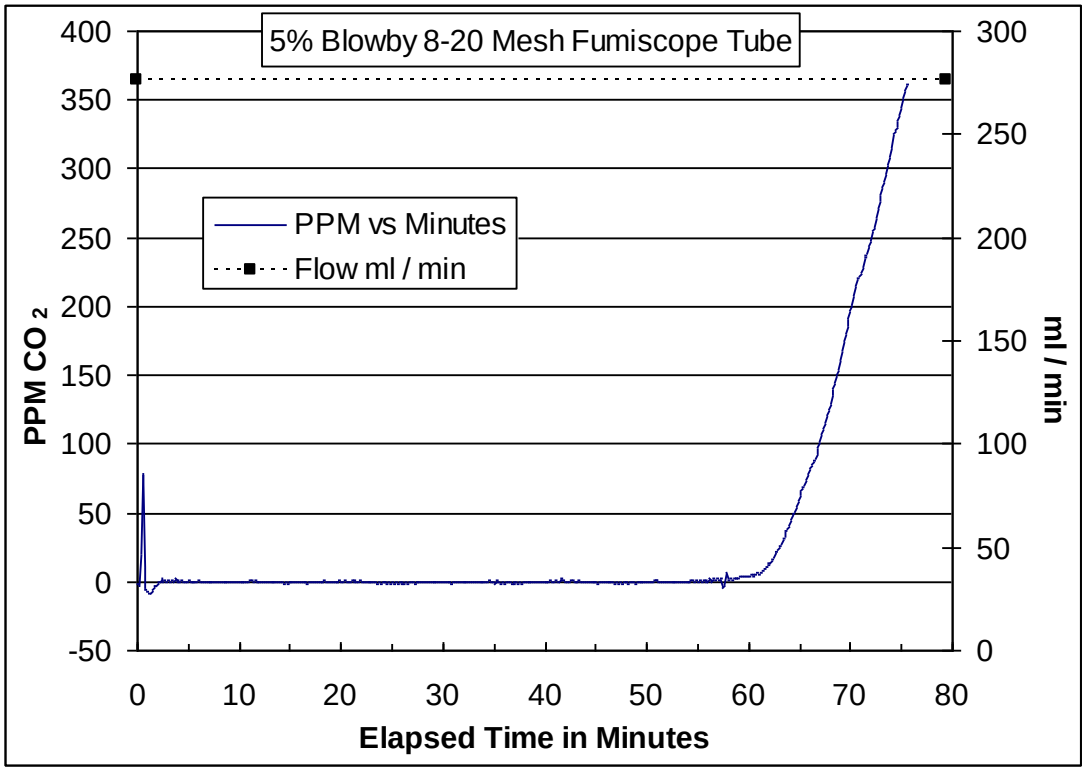


Figure 15.

Breakthrough of 5% CO_2 was observed after 57.5 minutes at a low flow rate of 272 ml/min. There was no need to adjust flow gauge to maintain steady flow rate. Virtually the entire content of the Ascarite II in the tube was utilized, as shown in the Appendix photos, compared with a 20-30 mesh tube after failure within less than 5 minutes (Figure 18).

Although we can force an artificially high flow rate by gauge adjustment, and still have no blow-by of the CO_2 this is not a practical solution to Ascarite tube life. Figure 16 shows this to be true, as a 472 ml/min (1.0 SCFH) flow rate, normal for the Fumiscope and maintained as long as possible, with 5% CO_2 in a glass 10g Ascarite tube, indicated no CO_2 breakthrough until about 24 minutes, though plugging began at about 17 minutes.

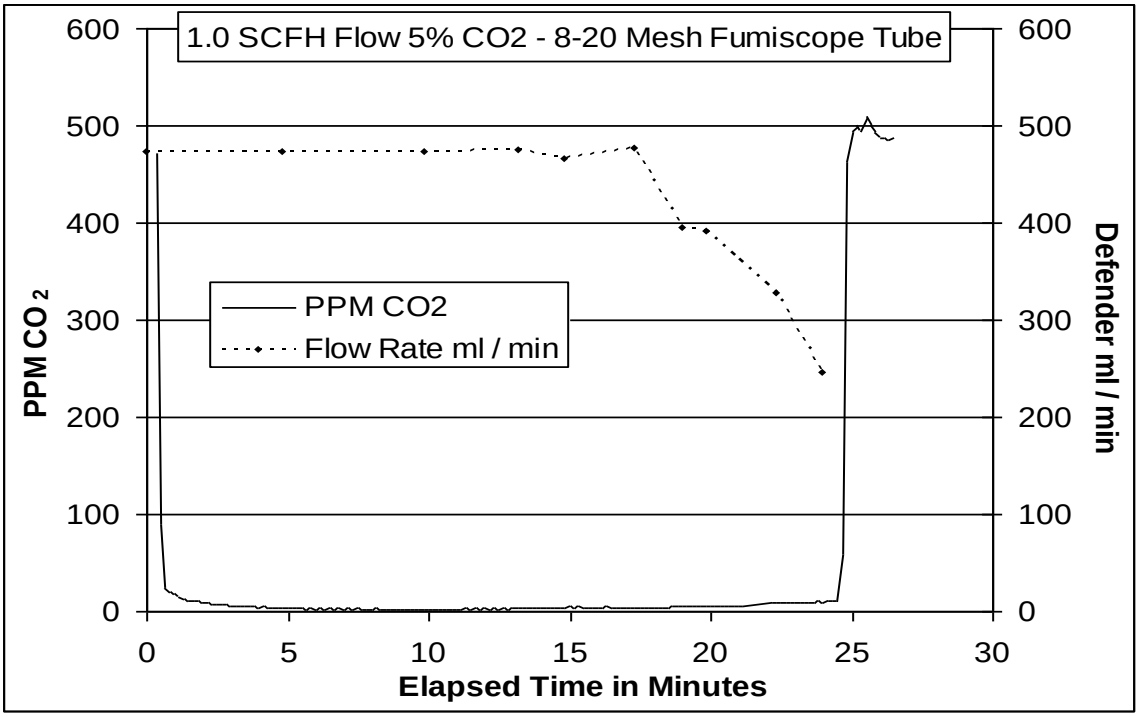


Figure 16. An steady initial air flow rate of 472 ml/min of 5% CO_2 and the corresponding breakthrough after 24 minutes.

Tests with Variable CO_2 Concentrations and 8-20 Mesh Ascarite II.

The previous tests indicated that the finer mesh Ascarite II (20-30 mesh) plugged up very quickly. Tests with the 8-20 mesh Ascarite II were conducted at CO_2 concentrations of 0.5. 2.0, 3.0, 4.0 and 5.0 %. During the course of the tests, the Fumiscope flow rate was constantly adjusted to maintain a 1.0 SCFH flow rate. Data was recorded as elapsed minutes, Fumiscope flow gauge reading, the Defender calibrator flow range, the mm Hg vacuum as read form the Dwyer manometer, and the Fumiscope reading of the MeBr setting. This would simulate a field usage, where PPQ Officers use a Fumiscope, and maintain the 1.0 SCFH flow rate. The results of this test are shown in the Figure17-21 shown below. Photographs of the condition of the glass Ascarite tubes used with 8-20 mesh Ascarite II in these tests are shown in Appendix I.

Tests with 0.5% CO_2, 8-20 mesh Ascarite II.

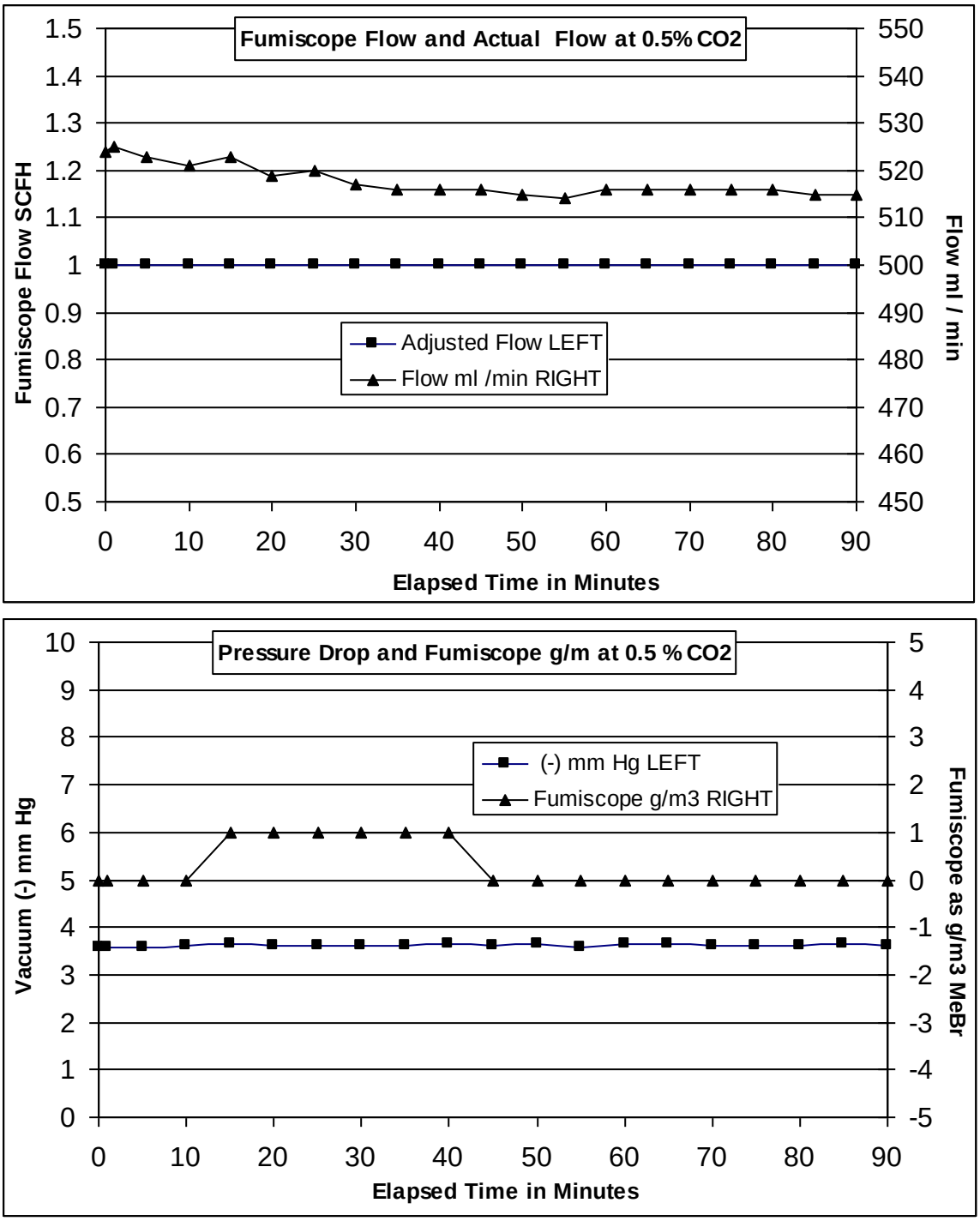
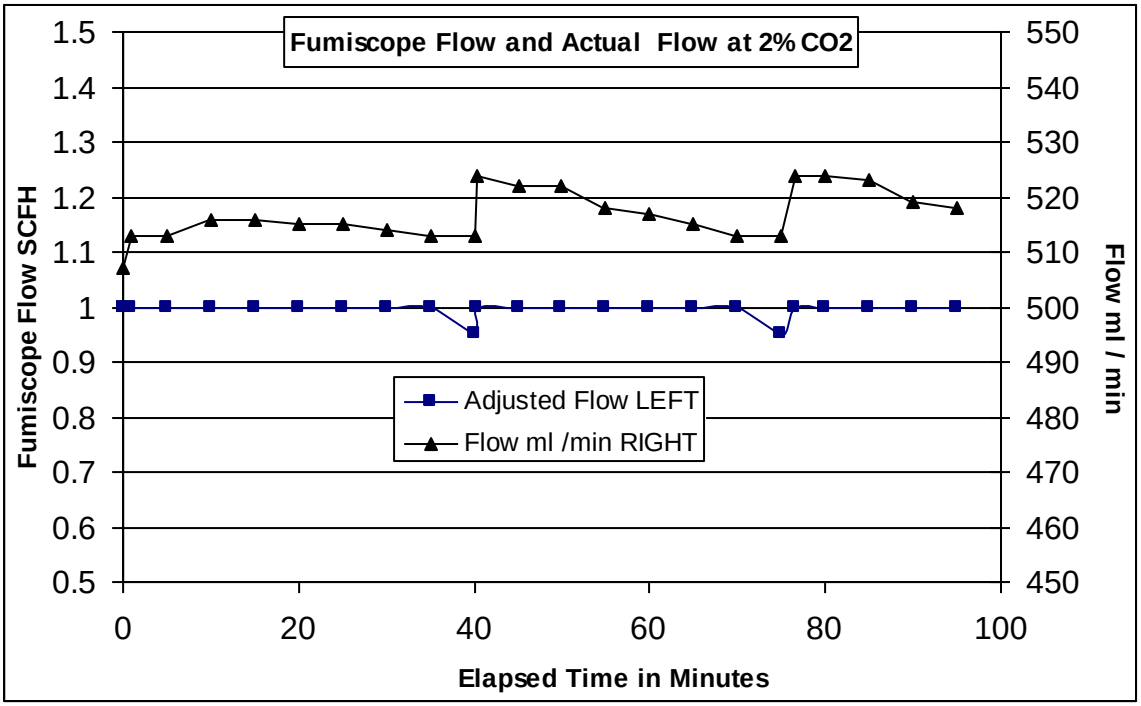


Figure 17. *Upper*. At lowest CO_2 concentration of 0.5% Fumiscope flow was maintained, but the Defender ml/min slightly declined over 90 minutes. *Lower*. System vacuum draw remained constant, while Fumiscope g/m3 as MeBr drifted up/down by 1. We can expect Ascarite tube life of about 90 minutes at this concentration.

Tests with 2.0% CO_2, 8-20 mesh Ascarite II.



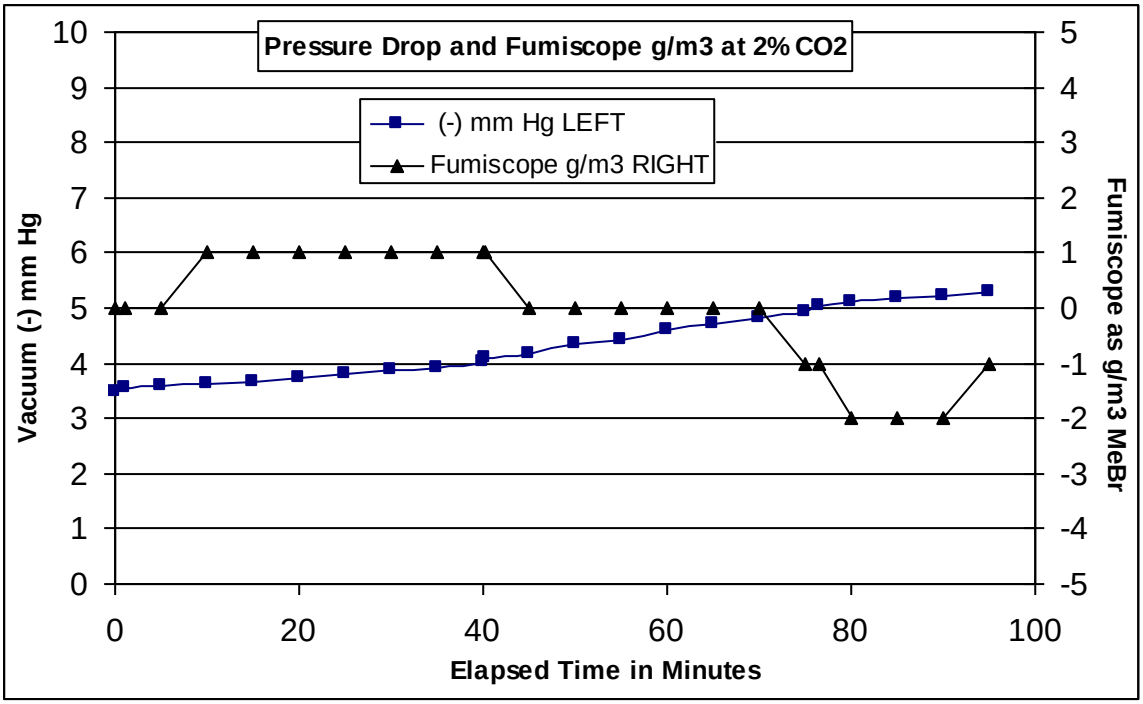
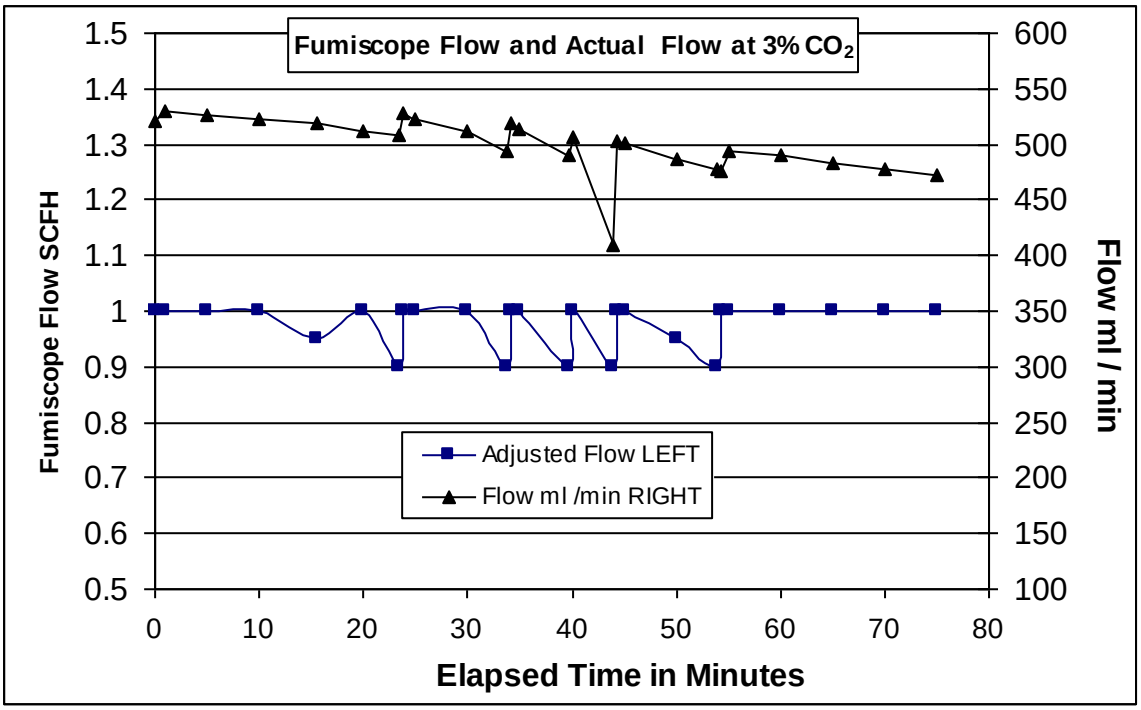


Figure 18. *Upper*. At a concentration of 2% CO_2 Fumiscope flow needed to be adjusted upward twice, and the Defender flow reflected that. *Lower*. Increase in Fumiscope pump power caused the system vacuum to increase, causing instability reflected by the drift in Fumiscope g/m3 on the MeBr scale. We can expect Ascarite tube life of about 70 minutes at this concentration.

Tests with 3.0% CO_2, 8-20 mesh Ascarite II.



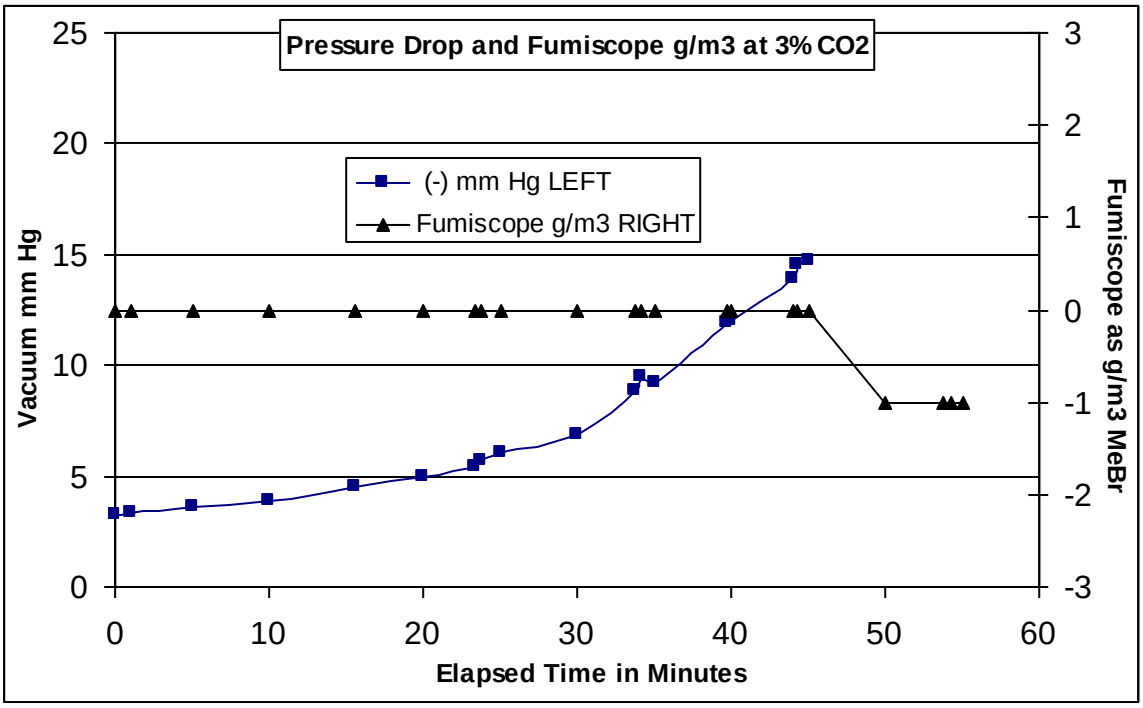
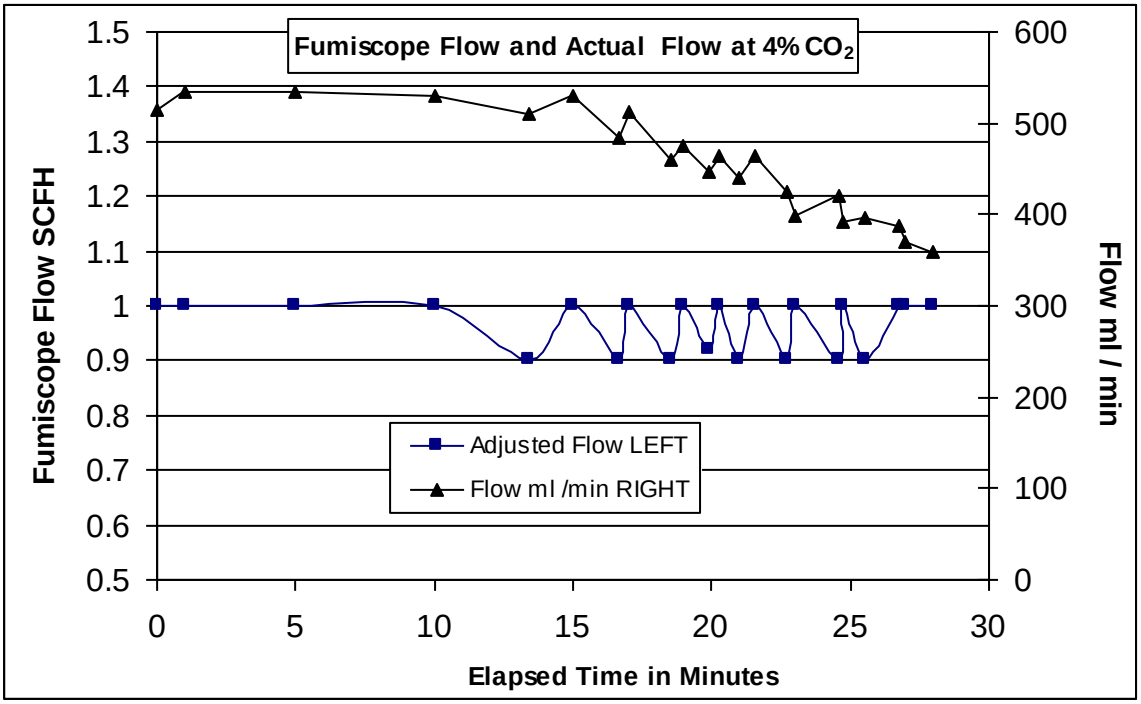


Figure 19. *Upper.* At a concentration of 3% CO_2 Fumiscope flow needed to be adjusted constantly after about 20 minutes, and the Defender flow reflected those changes. *Lower.* The frequent increased in Fumiscope pump power caused the system vacuum to increase quickly, which correlated with Fumiscope drift after vacuum reached about (-) 12 mm Hg. At this concentration, we should expect Ascarite tube life of about 40 min.

Tests with 4.0% CO_2, 8-20 mesh Ascarite II.



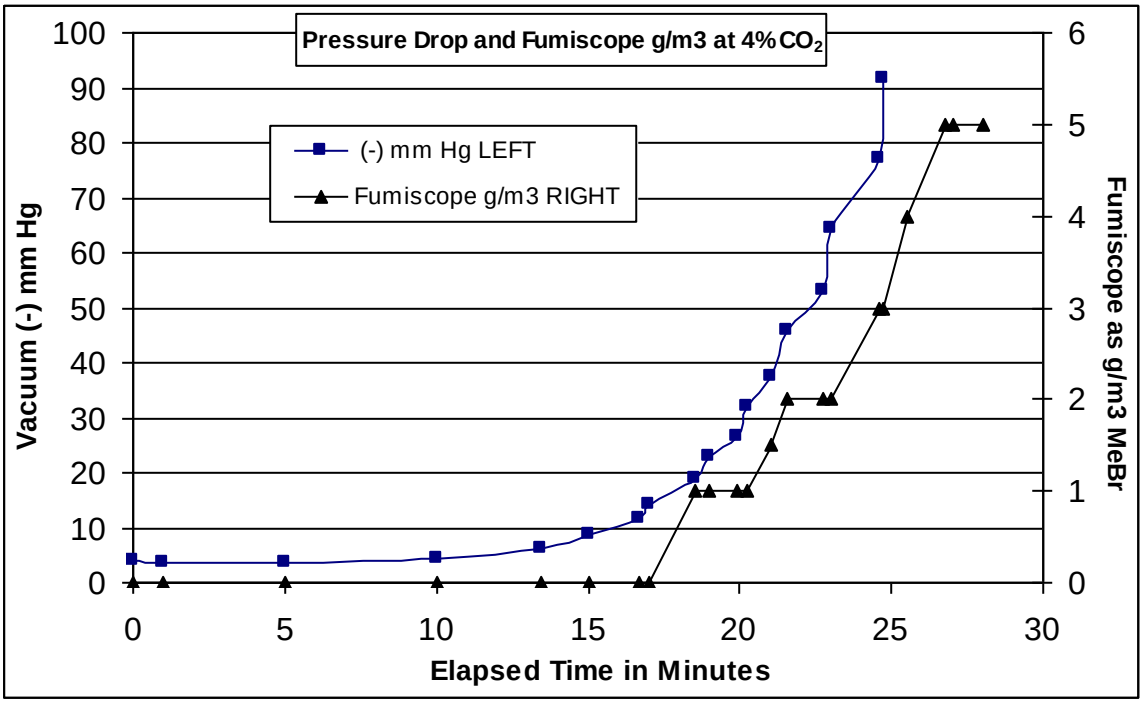
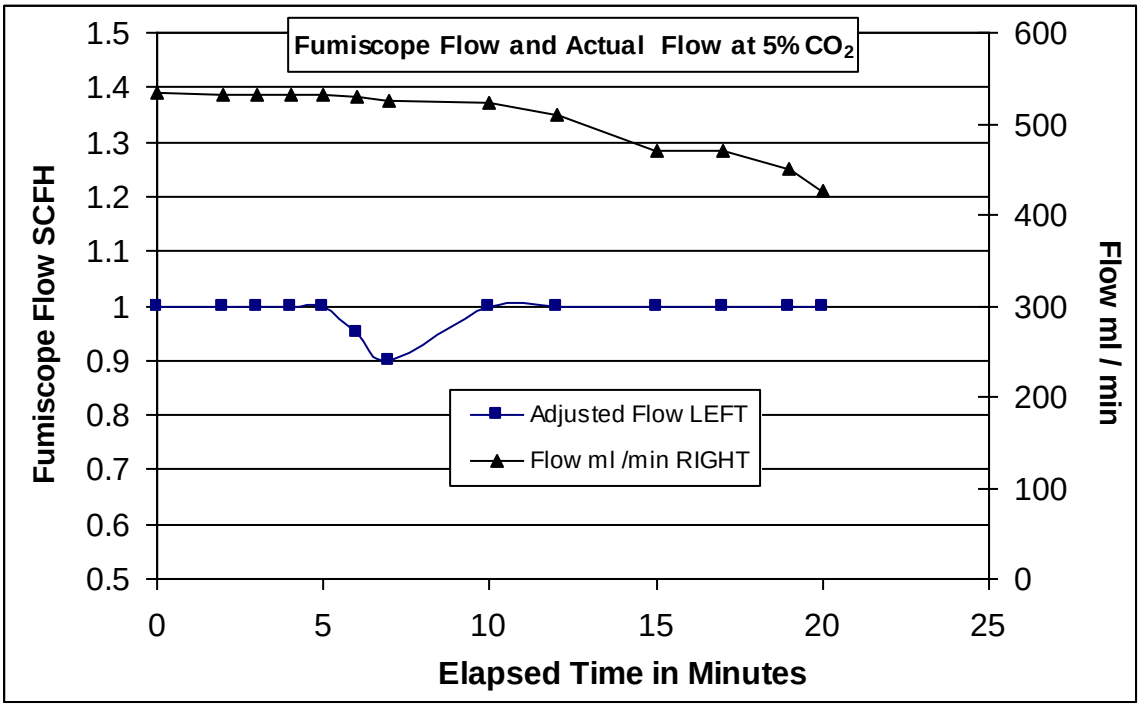


Figure 20. *Upper.* With a CO_2 concentration of 4% Fumiscope pump adjustments were constantly required after about 10 minutes, and real flow rate as indicated by the Defender show this. *Lower.* As a result, system vacuum increased rapidly after that point, with a corresponding increase in false Fumiscope readings. Ascarite tube life at 4% CO_2 should be expected to be no longer than about 15 minutes.

Tests with 5.0% CO_2, 8-20 mesh Ascarite II.



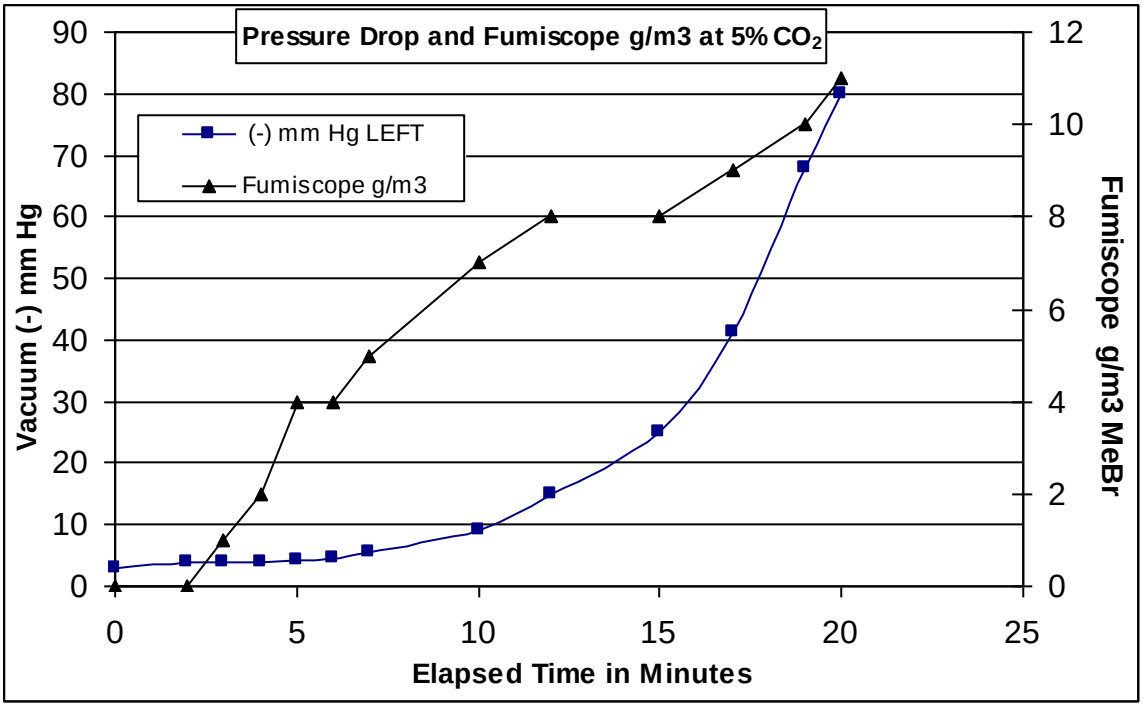


Figure 21. *Upper.* With a CO_2 concentration of 5%, constant and continuous Fumiscope pump adjustments were required to keep flow at 1.0 SCFH after 5 minutes, and the decline in real Defender flow rate shows this. *Lower.* The system vacuum increased dramatically, and Fumiscope false readings increased. At 5% CO_2, Ascarite tube life can be expected to be only 5 minutes or less, and is therefore not useful.

Conclusion.

The use of Ascarite II as a CO_2 scrubber used with the Fumiscope has useful value, but it is seriously affected by concentration and Ascarite mesh. We cite the following evidence:

1. Ascarite II of either coarse or fine mesh is very efficient at scrubbing CO_2, but this only applies practically if flow and pump pressure can be maintained at suitable low levels.

2. Ascarite II of fine 20-30 mesh is only useful at very low CO_2 concentrations, as the large reaction surface allows the scrubbing front to concentrate in the upper portion, thus wasting the remainder, as well as causing air flow restrictions. At high concentrations, plugging happens very fast.

3. Ascarite II of 8-20 mesh allows the reaction to proceed further and faster down the tube, however, plugging will eventually occur. A mesh size of 8-20 is necessary at higher concentrations.

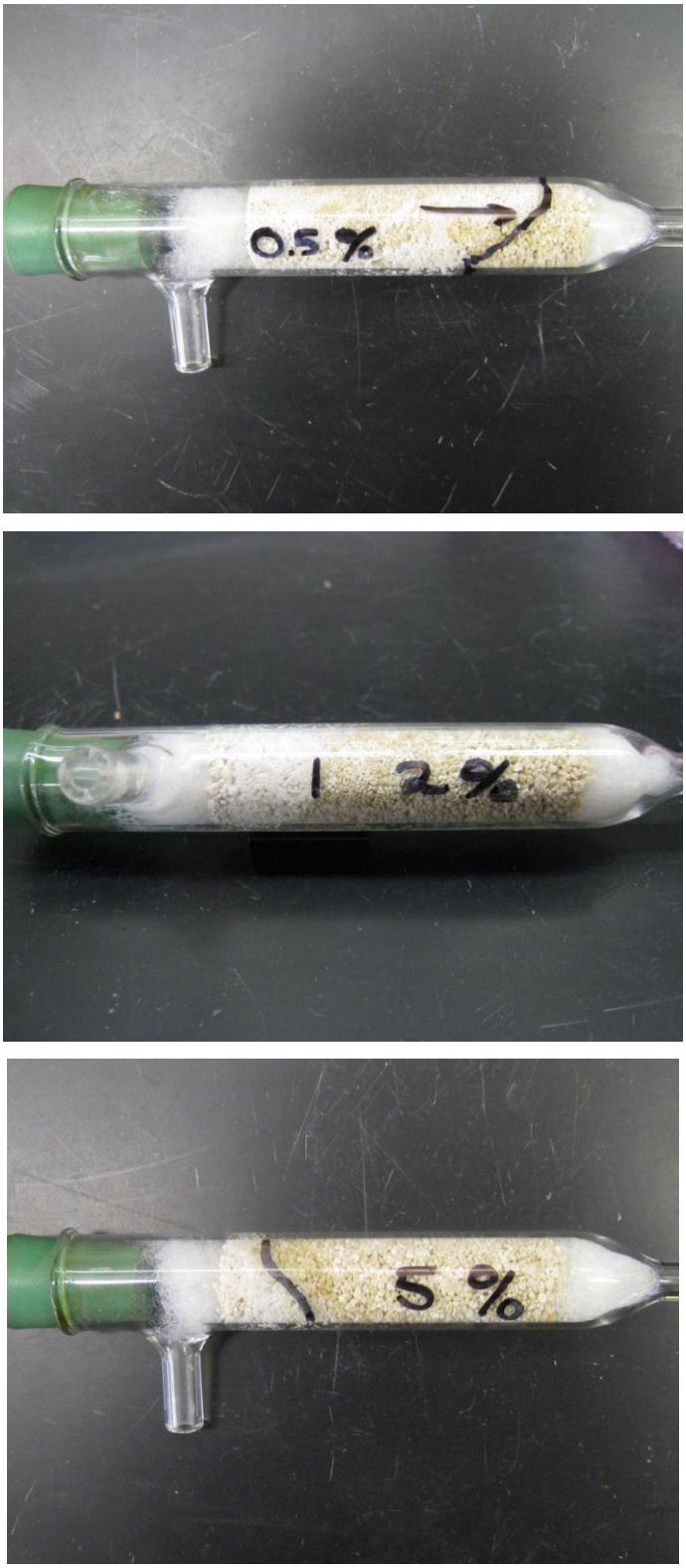
4. Tube life should not be extended beyond time at which Fumiscope flow (and therefore vacuum) drops below 0.8 SCFH (from original 1.0 SCFH setting). This may occur near the end of the tube contents. Increasing the flow at this point may cause erroneous false readings and overload Fumiscope pump.

5. The Ascarite II reaction region, as evidenced by a white reaction product, may reach about 75% of the length of a 10 g Ascarite II charge before plugging makes change necessary. The reaction front extends further down the tube than the solid white band, which indicated near total consumption with increased plugging.

Table 1. Approximate life of Ascarite II in glass tube. This can vary with packing of the, amount of Ascarite due to tube variability, amount of glass wool used, and exact CO_2 concentration. At low concentrations, the reaction is not highly exothermic, and therefore proceeds more slowly, apparently allowing long life for 20-30 mesh at low concentrations.

% CO_2	Ascarite II Product, in Glass Tube	
	8-20 mesh, 10 g	20-30 Mesh, 10 g
0.5	90 min.	up to 2 hrs.
1.0	80 estimate	90
2.0	70	10 min. Do Not Use
3.0	40	6 min. Do Not Use
4.0	20	< 3 min. Do Not Use
5.0	< 5 min. Do Not Use	< 3 min. Do Not Use

Appendix I. Ascarite tubes used to conclusion, with 10 g of 8-20 mesh Ascarite II after trials with several concentrations of CO_2.



Appendix II.

Equipment used.

1. Fumiscope, with internal drying system, and associated glass Drierite/Ascarite II tubes. Associated silicone and Tygon® connecting tubing.

   Key Chemical Company
   13195 49th Street N Ste. A
   Clearwater, FL 33762
   727-572-1159

2. Drying tube, Number 26930. Indicating Drierite.

   W. A. Hammond Drierite Company, Ltd.
   P.O. Box 460
   Xenia, OH 45385
   937-376-2927

3. Ascarite II. 8-20 Mesh and 20-30 Mesh. Used in glass "Fumiscope tubes" (10 g capacity) and in polycarbonate tubes (30 g capacity).

   Thomas Scientific
   P.O. Box 99
   Swedesboro, NJ 08085
   856-467-2000

4. Qubit CO_2 Analyzer, Model S157. With Logger-Pro Software and Go-Link Interface. 0-2000 ppm range.

   Qubit Systems Inc.
   700 Gardiners Road, Unit 105
   Kingston, Ontario
   Canada K7M 3X9
   613-384-1977

5. Precision air flow meter. Ball type rotameter. Model 7160 PTFE precision valve.

   Gilmont Instruments
   28W092 Commercial Avenue
   Barrington, Illinois 60010
   1-800-962-7142

6. Bios Defender 510 precision air flow calibrator.

Bios International Corporation
10 Park Place
Butler, NJ 07405
973-492-8400

7. Dwyer precision digital manometer. Model 477-2.

Dwyer Instruments, Inc.
102 Highway 212
Michigan City, IN46361-0373
219-879-8000

8. Calibration gas. Certified ± 2.0% Carbon dioxide in several concentrations from 0.5 through 5.0 %.

Airgas South, Inc.
5480 Hamilton Blvd.
Theodore, AL 36582
251-653-2530

9. Gas bags, non-sorptive Tedlar®, up to 100 liter capacity.

SKC, Inc.
863 Valley View Road
Eighty Four PA, 15330
724-941-9704

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MeBr Monitors: Response under cold conditions.

Any gas is subject to changes in atmospheric pressure and temperature. While the ppm of a mixture remains constant, molecular density (g/m^3, mass density) will increase with an increase in pressure and a decrease in temperature. The magnitude of the change is proportional to pressure in atmospheres (1 atm. = 760 mm Hg at sea level) and temperature Kelvin (Kelvin = °C + 273.15).

Two fumigant monitors approved by APHIS for quarantine fumigation were tested with custom standards prepared with 100% Q-label MeBr or a certified calibration gas of 20,720 ppm ± 1% MeBr. At 760 mm Hg and 23°C, this mixture had a MeBr density of 80.95 (80.14-81.76) g/m^3, as calculated with the ideal gas law where PV = nRT and a gas constant of 0.0820575 liter-atm/mole/K.

Tests with the Spectros ContainIR. MeBr standards were prepared according to the table below. The ppm to g/m3 conversion was calculated, and compared with the ContainIR reading for each concentration. The result is presented graphically following the Chart. Linearity over a wide range was excellent. A small tail-off at very low doses was affected more by 0.1 g/m^3 differences as a percent of value than with higher doses. Rounding errors at these low doses therefore had a greater effect, though small in terms of real differences. The operating characteristics and sensitivity of an IR cell designed to operate at more useful concentrations, as well as absorbance sensitivity of particular gasses, can contribute to less sensitivity at the extremes low range. This unit was non-responsive to atmospheric CO_2 up to 100,000 ppm.

P	Temp.	PPM per	Air	MeBr	PPM	g/m3	Spectros	Difference
mm Hg	°C	g/m3	ml	ml	Calc.	Calculated	IR-g/m^3	Calc-IR
757.1	23.4	257.27	2000	5	2,494	9.7	9.4	-0.3
757.1	23.4	257.27	2000	10	4,975	19.3	18.8	-0.5
757.1	23.4	257.27	1980	20	10,000	38.9	38.3	-0.6
757.1	23.4	257.27	1960	40	20,000	77.7	77.8	0.1
757.1	23.4	257.27	1940	60	30,000	116.6	116.8	0.2
757.1	23.4	257.27	1920	80	40,000	155.5	155.8	0.3
757.1	23.4	257.27	1900	100	50,000	194.4	195.6	1.2
757.1	23.4	257.27	1560	100	60,241	234.2	233.8	-0.4
757.1	23.4	257.27	1990	150	70,093	272.5	273.7	1.2
757.1	23.4	257.27	1720	150	80,214	311.8	313.1	1.3
756.2	23.1	257.31	2000	198	90,082	350.1	348.5	-1.6
756.2	23.1	257.31	1800	200	100,000	388.6	389.5	0.9

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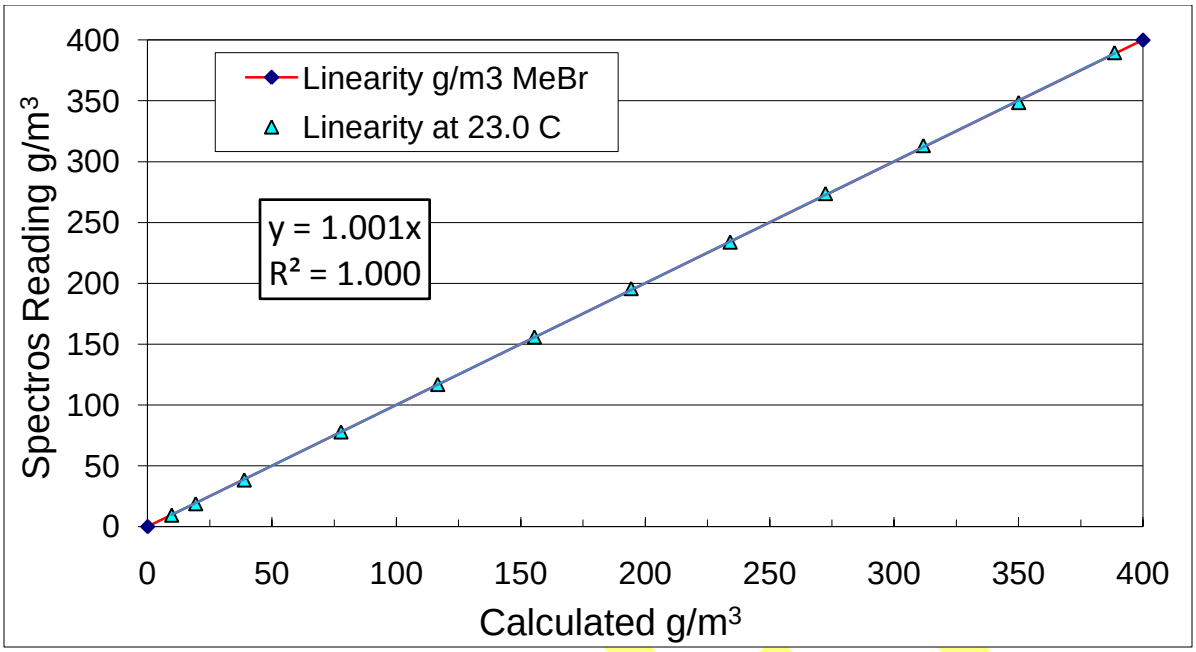

At each of several concentrations, the headspace temperature was reset from 23°C to 5, 10 or 16 C to check ability of the ContainIR to convert concentrations from instrument temperature to what would be the density of the mixture at each different chamber/headspace temperature. Standard gas was depleted before all readings could be taken, and some readings at 10 and 16°C may have ended slightly low due for this reason, accounting for small differences from computed vs. instrument reading. The result shows very good temperature correction to headspace temperature readings when the instrument was at different ambient temperature.

Contain-IR Entered Headspace T setting			*0.9346*	*0.9548*	*0.9750*	Differences from Computed Reading, At Headspace Temp		
			T Correction Factors					
4°C	**10°C**	**16°C**	**Computed Correction***			**4°C**	**10°C**	**16°C**
9.8	9.6	9.4	10.06	9.84	9.64	-0.26	-0.24	-0.24
19.9	19.5		20.12	19.69		-0.22	-0.19	
40.9	40.1	39.2	40.98	40.11	39.28	-0.08	-0.01	-0.08
83	81.4		83.25	81.48		-0.25	-0.08	
124.3	121.8		124.98	122.33		-0.68	-0.53	
165.7	160.2		166.71	163.17		-1.01	-2.97	
208.8	204.9		209.29	204.86		-0.49	0.04	
248.8			250.17			-1.37		
					Avg.	**-0.58**	**-0.62**	**-0.08**

* Based on proportion of set headspace Kelvin Temperature / K ambient of 296.55. Pressure was constant.

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Tests with a Fumiscope at 5°C and 23°C.

Scott-Marrin 20,720 ±1.0% ppm calibration gas was used to calibrate a Fumiscope at 81 g/m^3. At ambient conditions of 758.6 mm Hg and 23.8°C methyl bromide density was 80.86 ± 0.81 g/m^3. The Fumiscope was operated with a Hammond 30-g Drierite desiccant tube at all times.

1. Supply 5°C MeBr to a Fumiscope at 5.0°C. At 5°C and 754.5 mm Hg, the density of the MeBr was calculated to be 86.19 g/m3. A 25-liter SKC Tedlar gas bag was filled with the MeBr and allowed to chill for 2-h at 5.0°C. The Fumiscope was also placed in the cold chamber and allowed to reach stabile zero after the same time. The source of MeBr was then connected directly to the Fumiscope, and readings observed for 7.0 minutes.

2. Supply 22.8°C MeBr to a Fumiscope at 5.0°C. The Fumiscope was kept in the cold chamber, and the MeBr was maintained at room ambient of 22.8°C. The MeBr was allowed to acclimate for 1-h before connecting directly to the Fumiscope. Readings were observed for 7.0 minutes.

3. Supply MeBr gas to Fumiscope at ambient. After 2-h to reach ambient temperature, MeBr at 23.7°C and 754.5 mm Hg was supplied to the Fumiscope. Under these conditions, MeBr was at a computed density of 80.76 g/m^3. The gas was directly connected to the Fumiscope.

4. Post-test check. Following the tests, the unit was checked for accuracy against fresh calibration gas. The Fumiscope reached 80 g/m3 after 10 minutes, and 81 g/m^3 after 13 minutes. Some drift of ±1 g/m^3 has been observed in the past. An instrument that reads out in whole numbers is inherently less precise, and rounding error may also contribute to small changes attributed to drift. Further, best accuracy is obtained after operation longer than is ideal for field use (5-7 min. or more).

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Results of Fumiscope tests.

MeBr /Fumiscope Conditions	Time to 1 g/m^3	Time to 80 g/m^3	Highest g/m^3	Last g/m3	Target g/m^3 (expected)
5°C MeBr 5°C Fumiscope	0:31	2:19	83 g/m^3 3:08	82 g/m3 5:00-6:00	86
22.8 °C MeBr 5 °C Fumiscope	0:31	3:03	81 g/m^3 3:41	80 g/m3 6:00-7:00	81
23.7°C MeBr 23.7°C Fumiscope	0:30	5:14	80 g/m^3 5:14	80 g/m3 6:00-7:00	81

Since 20,720 ppm MeBr held at 5°C had a calculated density of 86.19 g/m3, it was apparent that the Fumiscope also at 5°C was not able to accurately read the true concentration. The maximum reached was 83 g/m3, followed by a drift to 82 g/m3. This is likely due to the internal temperature of the Fumiscope slightly warming (making less dense) the gas sample. Ambient warm gas supplied to a cold Fumiscope was practically near expected values (-1) as the operating temperature of the Fumiscope likely somewhat overcame cold environment. At lab ambient, expected values were again reached, considering small drift due to instrument, flow, and ambient P and T may be slightly variable but calculable. It is obvious that when monitoring a fumigation at temperatures colder than the Fumiscope (and more importantly during calibration) a correct reading of concentration is not possible without internal compensations or manual calculations based on ambient P and temperature differences. In situations where large differences may occur, a thermal conductivity instrument may under-report actual concentrations.

The table below compares ambient temperature (assumed to be input gas temperature) with exhaust temperature of a Fumiscope. Exhaust temperature in the cell could possibly be slightly higher, since exhaust was measured at output. A Fumiscope was placed in a cold room or ambient room and monitored by thermocouple inserted into the exhaust port after one hour of continuous operation. The same thermocouple/reader was used for both measurements.

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Instrument Temperature °C	Exhaust Temperature °C	Instrument Increase °C
22.6	25.9	3.3
3.6	7.0	3.4

Temperature effects would be in addition to the effect of pressure drops (without internal pressure compensation) due to long sample lines and sample line sorption at slow flow rates, as shown in previous tests.

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Comparisons of Spectros IR Monitor with the Fumiscope or Thermal Conductivity Instrument: Issues and procedures.

Calibration Error.

1. Spectros Calibration. The Spectros unit is factory calibrated, based on molecular concentration. It automatically compensates for ambient pressure and temperature with built-in programming. Large differences in pressure or temperature during calibration can be easily be introduced by weather patterns of the day of calibration.

2. Fumiscope Calibration. When calibrating a thermal conductivity (TC) instrument, a known ppm gas is used. This gas will vary in density (g/m^3) with ambient temperature and pressure.

Pressure Effects.

1. Spectros IR. The Spectros has internal pressure compensation. A sample of gas, due to pump pressure, will be different than ambient headspace pressure, therefore air density. Increasing sample leads require more pump pressure, and therefore affects air density proportionally.

2. Fumiscope. There is no pressure compensation ability. Measuring pressure of input/output air with 0, 100, 200, 300 feet of 0.25 inch LDPE sample line has indicated that pressure error of 1.5 % can be introduced with 300 feet of tube, and is proportional to tube length. In real terms, that can easily exceed 1 g/m3 in typical produce fumigation.

Temperature Effects.

1. IR Temperature effects. Spectros monitors compensate for temperature differences between headspace sample and instrument temperature. As gas warms, it becomes less dense, and will alter a reading by 1.01 % for each 3°C difference. Spectros compensates for this by prompting for entry of headspace sample temperature.

2. Fumiscope temperature effects. The Fumiscope does not compensate for temperature differences during sampling fumigations at different temperatures. An example of this is when leads are from a 40°F fumigation headspace, and the unit is in a heated room at 70°F. An error of 2.72 g/m3 in a 48 g/m3 fumigation can be introduced (5.66%).

Competing gasses.

1. Spectros uses IR technology. IR technology is not affected by competing gasses such as CO_2 or ethylene. IR technology is specific to a wavelength that is absorbed by MeBr. There is no need for Ascarite for CO_2 or Drierite to remove moisture.

2. With TC technology, air density is increased by CO_2. For every 1% of CO2, the Fumiscope will register MeBr as 12 g/m3 higher than actual levels. Scrubbing this CO_2 by means of Ascarite is problematic. Ascarite is very hazardous, expensive, and difficult to use. It also complicates the re-zeroing process. The accuracy of CO_2 scrubbing will be affected by the amount and condition of scrubber used. Ascarite and Drierite retain residual MeBr, thus making re-zeroing difficult.

Speed of Operation.

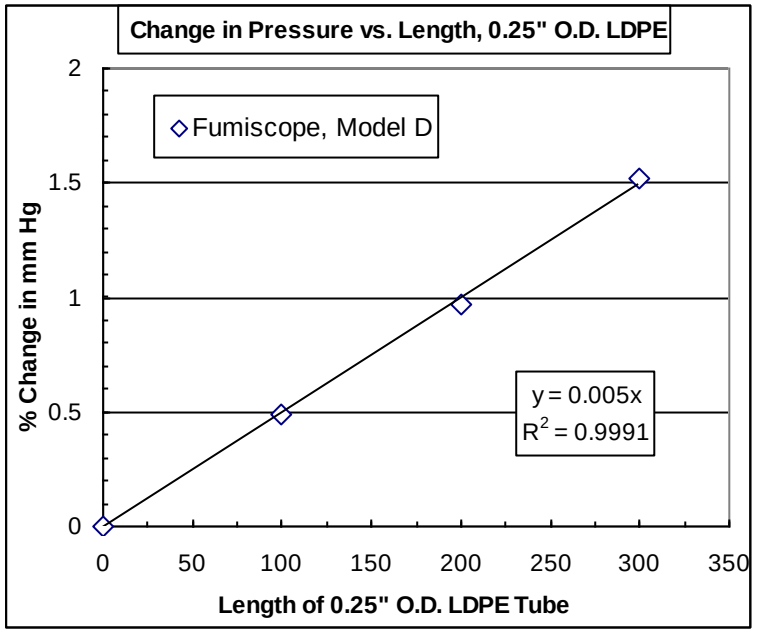
1 The Spectros IR unit will sample about 1.5 liters per minute. This allows fast purging of leads. The self-calibrating and purging cycle allows readings to be taken in about a minute in some situations. Self-purging/re-zeroing is fast, taking about 15 seconds. The unit is exceptionally very fast if sample lines are purged with auxiliary pump. For example, ½ hour readings will be on time, instead of 15 or more minutes late.

2. The Fumiscope processes sample air at about 1 SCFH (0.472 L-min.). In addition, it takes a long time to reach true value due to its slow rate of sample. Several minutes are required for full reading. Re-zeroing time is long, often taking several minutes. Accurate re-zeroing requires similar length of tubing compared with sample lines to avoid pressure complications, and consistent quality and quantity of Ascarite or Drierite.

Topic/Feature	Spectros MB-ContainIR® Monitor	Thermal Conductivity Fumiscope®
Initial Cost	$5,000.00 per unit. Service contract, replacement, recalibration option	$2,000.00 per unit.
Long Term Costs	Factory calibration, repair.	Expendables (Ascarite, Drierite) Repair, recalibration.
Calibration Error.	The ContainIR unit is factory calibrated, based on molecular concentration. It compensates for ambient pressure and temperature utilizing built-in programming. Large differences in pressure or temperature during calibration can be easily be introduced by weather patterns of the day of calibration.	When calibration is based on gas density at time of calibration, a permanent error of about 1.01% for every 3°C difference, and 1% for every 7.6 mm difference, in pressure from the 24 °C /760 mm Hg standard. This error will add or subtract, *permanently until recalibrated*, a fixed g/m^3 error that can easily be as much as 2-3 g/m^3. That is over 5% in 56-g fumigation.
Pressure Effects	The ContainIR has internal pressure compensation. A sample of gas, due to pump pressure, will be different than ambient headspace pressure, therefore air density. Increasing sample leads require more pump pressure, and therefore affects air density proportionally.	There is no pressure compensation ability. Measuring pressure of input/output air with 0, 100, 200, 300 feet of 0.25 inch LDPE sample line has indicated that pressure error of 1.5 % can be introduced with 300 feet of tube, and is proportional to tube length. In real terms, that can easily exceed 1 g/m3 in a typical produce fumigation.
Temperature Effects	ContainIR units compensate for temperature differences between headspace sample and instrument temperature. As gas warms, it becomes less dense, and will alter a reading by 1.01 % for each 3°C difference. Spectros compensates for this by prompting for entry of headspace sample temperature.	The Fumiscope does not compensate for temperature differences during sampling fumigations at different temperatures. An example of this is when leads are from a 40°F fumigation headspace, and the unit is in a heated room at 70°F. An error of 2.72 g/m3 in a 48 g/m3 fumigation can be introduced (5.66%).

Competing Gasses	IR technology is not affected by competing gasses such as CO_2 or ethylene. IR technology is specific to a wavelength that is absorbed by MeBr. There is no need for Ascarite® for CO_2 or Drierite® to remove moisture.	For every 1% of CO2, the Fumiscope will register MeBr as 12 g/m3 higher than actual levels. Scrubbing this CO_2 by means of Ascarite is problematic. Ascarite is very hazardous, expensive, and difficult to use. It also complicates the re-zeroing process. The accuracy of CO_2 scrubbing will be affected by the amount and condition of scrubber used. Ascarite and Drierite retain residual MeBr, thus making re-zeroing tedious, time consuming and difficult.
Speed of Operation	The Spectros IR unit will sample about 1.5 liters per minute. This allows fast purging of leads. The self-calibrating and purging cycle allows readings to be taken in about a minute in some situations. Self-purging/re-zeroing is fast, taking about 15 seconds. The unit is exceptionally very fast if sample lines are purged with auxiliary pump. For example, ½ hour readings will be on time, instead of 15-30 or more minutes late with multiple leads.	The Fumiscope processes sample air at about 1 SCFH (0.472 L-min.). In addition, it takes a long time to reach true value due to its slow rate of sample. Several minutes are required for full reading. Re-zeroing time is long, often taking several minutes. Accurate re-zeroing requires similar length of tubing compared with sample lines to avoid pressure complications, and consistent quality and quantity of Ascarite or Drierite. This can raise contamination issues because of tubing residual MeBr.
Ease of Operation	Plug in, warm up is fast, fast reading, no additional precautions.	User must be cognizant of condition of Ascarite, Drierite temperature differences, sufficient warm-up, delicate re-zeroing, frequent re-zeroing, sufficient line purges.
Battery Operation	Standard, 10-12 hr continuous between charges. 110-220 input for international use.	Not Standard. 110 V required, but additional inverter can use 12 V automotive sources.
Durability	Very durable. Passes ASTM D5276-98(2004) Standard drop test. Field replacement guaranteed if necessary.	Unknown. Suspected loss of calibration in shipping and rough use. Not drop-tested.
Warm-up Required.	15 minute built in. Can be bypassed if unit is disconnected from power briefly.	Undetermined, indefinite, insufficient warm up will affect drift and zero.
Precision.	Accurate to 0.1 to 1% or better within practical mid-ranges. 2-2.5 % at extreme range of over 300 g/m^3 to over 400 g/m^3.	Reads to 1 g/m^3. This also affects accuracy of calibration, by ±0.5 g/m^3.

Environmentally Influenced Errors.	The ContainIR is shielded against EMF (transformer effect from AC current nearby), fluorescent lighting, cell phone, air pump and static electric effects on cell.	Fumiscope has no EMF or other protection against electrical interference. Wire windings in a TC cell are subject to these influences within a 4 ft distance up to 10 ft.
Best use.	All applications. Best where CO_2 is an issue, such as green wood, certain produce under warm conditions. Accurate at low concentrations, where phytotoxicity is critical. May reduce use of additional MeBr due to accuracy.	Not as versatile. Not optimum when CO_2, humidity, weather conditions variable, at higher elevations.
Recommendation	This unit is not subject to additive errors due to calibration, variation in ambient pressures and temperatures, condition of ancillary materials, improper re-zeroing, or loss of calibration due to handling.	Subject to many possible errors, all of which are additive and can be significant.
Sulfuryl Fluoride	USDA is in possession of sulfuryl fluoride monitors of same design. They have research-level accuracy, and have been used successfully in this regard.	A Fumiscope cannot be used with sulfuryl fluoride in the presence of CO_2. SF is acidic, and will react and be scrubbed by Ascarite, thus giving very low false readings. This will be true for any acidic fumigant gas.
Future Developments	Modules will be available for internet reporting, remote control of solenoid gas valves, telephone notification of error, etc.	Some capability, but operational requirements make this impossible if Ascarite is needed for CO_2 scrubbing.


Change in Pressure vs. Length, 0.25" O.D. LDPE
Fumiscope, Model D
y = 0.005x
R2 = 0.9991
% Change in mm Hg
Length of 0.25" O.D. LDPE Tube
0
0.5
1
1.5
2
0
50
100
150
200
250
300
350

G/M3 to PPM												1 ATM		
			ATM	0.96225	0.96718	0.97212	0.97705	0.98199	0.98692	0.99186	0.99679	1.0000	1.00173	1.00666
			mbar	975.00	980.00	985.00	990.00	995.00	1000.00	1005.00	1010.00	1013.25	1015.00	1020.00
			mm Hg	731.3	735.1	738.8	742.6	746.3	750.1	753.8	757.6	760.0	761.3	765.1
Temp°C	Temp°F	Temp°K	in Hg	28.79	28.94	29.09	29.23	29.38	29.53	29.68	29.83	29.92	29.97	30.12
1	33.8	274.16		246.23	244.98	243.73	242.50	241.28	240.08	238.88	237.70	236.94	236.53	235.37
2	35.6	275.16		247.13	245.87	244.62	243.39	242.16	240.95	239.76	238.57	237.80	237.39	236.23
3	37.4	276.16		248.03	246.76	245.51	244.27	243.04	241.83	240.63	239.44	238.67	238.26	237.09
4	39.2	277.16		248.93	247.66	246.40	245.16	243.93	242.71	241.50	240.30	239.53	239.12	237.95
4.44	40.0	277.6		249.32	248.05	246.79	245.55	244.31	243.09	241.88	240.68	239.91	239.50	238.32
5	41.0	278.16		249.83	248.55	247.29	246.04	244.81	243.58	242.37	241.17	240.40	239.98	238.80
6	42.8	279.16		250.72	249.45	248.18	246.93	245.69	244.46	243.24	242.04	241.26	240.84	239.66
7	44.6	280.16		251.62	250.34	249.07	247.81	246.57	245.33	244.11	242.90	242.12	241.71	240.52
8	46.4	281.16		252.52	251.23	249.96	248.70	247.45	246.21	244.98	243.77	242.99	242.57	241.38
9	48.2	282.16		253.42	252.13	250.85	249.58	248.33	247.08	245.85	244.64	243.85	243.43	242.24
10	50.0	283.16		254.32	253.02	251.74	250.46	249.21	247.96	246.73	245.50	244.72	244.30	243.10
11	51.8	284.16		255.22	253.91	252.62	251.35	250.09	248.84	247.60	246.37	245.58	245.16	243.96
12	53.6	285.16		256.11	254.81	253.51	252.23	250.97	249.71	248.47	247.24	246.45	246.02	244.81
13	55.4	286.16		257.01	255.70	254.40	253.12	251.85	250.59	249.34	248.11	247.31	246.88	245.67
14	57.2	287.16		257.91	256.59	255.29	254.00	252.73	251.46	250.21	248.97	248.17	247.75	246.53
15	59.0	288.16		258.81	257.49	256.18	254.89	253.61	252.34	251.08	249.84	249.04	248.61	247.39
15.55	60.0	288.71		259.30	257.98	256.67	255.37	254.09	252.82	251.56	250.32	249.51	249.08	247.86
16	60.8	289.16		259.71	258.38	257.07	255.77	254.49	253.21	251.95	250.71	249.90	249.47	248.25
17	62.6	290.16		260.60	259.27	257.96	256.66	255.37	254.09	252.83	251.57	250.77	250.33	249.11
18	64.4	291.16		261.50	260.17	258.85	257.54	256.25	254.96	253.70	252.44	251.63	251.20	249.97
19	66.2	292.16		262.40	261.06	259.74	258.42	257.13	255.84	254.57	253.31	252.50	252.06	250.82
20	68.0	293.16		263.30	261.96	260.63	259.31	258.01	256.72	255.44	254.17	253.36	252.92	251.68
21	69.8	294.16		264.20	262.85	261.51	260.19	258.89	257.59	256.31	255.04	254.22	253.79	252.54
21.11	70.0	294.27		264.30	262.95	261.61	260.29	258.98	257.69	256.41	255.14	254.32	253.88	252.64
22	71.6	295.16		265.10	263.74	262.40	261.08	259.77	258.47	257.18	255.91	255.09	254.65	253.40
23	73.4	296.16		265.99	264.64	263.29	261.96	260.65	259.34	258.05	256.78	255.95	255.51	254.26
24	75.2	297.16		266.89	265.53	264.18	262.85	261.53	260.22	258.92	257.64	256.82	256.37	255.12
25	77.0	298.16		267.79	266.42	265.07	263.73	262.41	261.09	259.80	258.51	257.68	257.24	255.98
26	78.8	299.16		268.69	267.32	265.96	264.62	263.29	261.97	260.67	259.38	258.54	258.10	256.83
26.67	80.0	299.826		269.29	267.91	266.55	265.21	263.87	262.55	261.25	259.95	259.12	258.67	257.41
28	82.4	301.16		270.48	269.10	267.74	266.39	265.05	263.72	262.41	261.11	260.27	259.82	258.55

Technical Report

Fumiscope Use: Operation, Drierite desiccant use, and performance.

Requesting Group: Treatment Quality Assurance Unit, CPHST, Raleigh, NC

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Background

The APHIS PPQ treatment Manual has general guidelines for recommended use of the Fumiscope thermal conductivity gas analyzer. However, various aspects of its use have not been decisively proven or documented in the laboratory. Here, we look at warm-up times and Drierite use under varied conditions, as well as the best zeroing procedure to recommend. Four Models were tested, the oldest without internal drying system, one retrofitted with the system, one purchased with the system, and one newer with single – switch operation (pump and meter). Other aspects of performance, such as long lead operation, speed of readings and zeroing procedures, were evaluated.

Introduction.

Questions have arisen over the best technique concerning operation of the Fumiscope. (Key Chemical, Clearwater, FL). This is critical, since APHIS PPQ has a number of Fumiscope thermal conductivity instruments in use for routine monitoring of quarantine fumigations with methyl bromide (MeBr). The thermal conductivity instrument measures air density, and thus is affected by the total volatile load of a given air sample. This may include compounds such as carbon dioxide (CO_2) water vapor, and volatiles evolving form commodities undergoing fumigation. These compounds may increase in concentration while a commodity is sealed under a tarpaulin or in a fumigation chamber, as well as in a cargo container, or in very humid location with water vapor. Further, being an electronic device, uncertainties exist regarding instrument drift over time and warm-up time required. Also, the effect of drawing samples through long sample leads is unknown at this time.

Fumiscope instruments tested and referred to in this report:

1. "Old Model". This was an older Fumiscope without the internal drying system now standard on newer models. This unit requires the desiccant Drierite® (W. A. Hammond Drierite Co., Ltd. Xenia, OH) to dry the sample for proper operation. These were equipped with a glass "Drierite tube" which holds about 10 g of Drierite. This tube has also been used in conjunction with Ascarite, a CO_2 absorbent, to scrub CO_2 from the sample stream. In these tests we used the Hammond 26930 disposable Drierite tube, which held 32 g of 10-20 mesh material. This as with similar units below, are designed to operate and are calibrated at an air flow rate of 1.0 SCFH, as measured by the integral Dwyer air flow gauge.

2. "Old-Retro". This was an older Fumiscope as 1, above, retrofitted with the internal drying system by Key Chemical. The manufacturer claims that this eliminates the need for Drierite. This has yet to be confirmed by APHIS, and as a result, we continue to recommend the use of Drierite desiccant.

3. "New-2sw". This is a newer model, with original internal drying from the factory. It has, as with 1, 2 above, independent switching of the electronics and pump. It is possible to warm up this unit without continuous pump operation.

4. "New-1sw". This unit is similar to 3, above, except that it has a single power switch. Thus, it cannot warm-up without pump operation.

5. "Spectros". A ContainIR MeBr monitor from Spectros Instruments, configured for automatic 20 second purges and one minute measure cycles, with automatic pressure and temperature compensations.

Methods.

Several scenarios of possible use were tested for warm-up time. They are listed below. This covers several situations under which Fumiscopes will be used, including long inactivity, use on consecutive days, using previous zero settings, start up in cold temperature, and transported in cold weather to use in a warm room or monitoring site. In this report, a "cold start" refers to a unit turned on at the beginning after a period of non-use of 1-4 d. Blue-to- pink indicating Drierite desiccant in disposable tubes was used at all times. A "clean zero" refers to zeroing a Fumiscope with fresh Drierite uncontaminated with MeBr.

Part 1. Tests on warm-up and stability.

1. Warm-up from cold start at 23.1° using previous zero, not used several months.
2. Warm-up form cold start at 23.1, previous zero, and turned off 1-day.
3. Warm-up form cold start at 23.1, previous zero, and turned off 4-days.
4. Old model, in 4-h warmed up condition with increased RH, a Drierite test.
5. Warm up from cold start at 9.8°C, only older units re-zeroed, turned off 1-day.
6. Repeat cold start at 9.8°C, previous zero, turned off 1-day.
7. Warm-up of cold (9.8°C) units moved to 23.2°C, turned off 1-day.
8. Warm up electronics 30 minute, and then turn on pump (2-switch models).
9. Supply 95% RH air to warmed-up, stable Old Model over 3.5 hours.

10. Influence of a long leads (300 ft) on zeroing and stability.

Part 2. Tests with methyl bromide and long leads.

11. Performance of Fumiscope with short or long leads and Methyl Bromide.
12. Performance of Spectros and Fumiscope with sequential sampling.
13. Collection of exhaust gas to cross-check lower levels.

Part 1. Tests on warm-up and stability.

1. A 23.1°C cold start warm-up, no previous zero. All four units have been in laboratory storage and have not been used within the last month. All units were set up for simultaneous operation with an individually switched power outlet. All units were operated with the in-line Drierite column (Hammond, OEM #26930) that contained about 32 g 10-20 mesh Drierite, and which was allowed to be used in a vertical position (Figure 8). All units have been previously calibrated with 14,610 ppm MeBr and the span set to 56 g/m^3 MeBr at 23°C and a flow rate of 1.0 SCFH (472 ml/min) as indicated on the unit's flow gauge. Room temperature was 23.1°C ± 0.65 SD, and RH was 45.1% ± 2.18 as measured by a HOBO data logger (Onset Computer, Pocasset, MA).

After all units were in position and supplied with fresh Drierite tubes (regardless of any internal drying system) the units were switched on, immediately set to "zero", and allowed to run continually at the recommended flow rate. The reading was recorded at one minute intervals or as needed. After 18 minutes, when the unit's display became more stable, the units were re-zeroed. After recording changes, the units were again re-zeroed after 25 minutes. No further zeroing was done, and the test was terminated after 50 minutes due to apparent stability in readout after all units operated for 10-20 minutes without change. The result is shown in Figure 1. Flow rates of all four units were measured during operation, and were determined to be as follows with Fumiscope air flow gauge set at 1.0 SCFH:

Old Model: 444 ml/min.

Old-Retro:	422 ml/min.
New-2sw:	518 ml/min.
New-1sw:	437 ml/min.

Fumiscope readings continually increased for, startup values of 0 to 6-12 after 18 minutes. Following re-zero, the readings again gradually climbed to 1-4, and were re-zeroed. Readings again climbed to 1-5 over the next several minutes, finally becoming more stable after 30-40 minutes total. The span of changes during warm-up was between -3 to +12 on the MeBr scale, more if changes after re-zero were included. Drierite was 1/3 used after 45 minutes. New full tubes were attached, with no changes observed.

Results varied between instruments. The Old Model (requires external Drierite) warmed up with least displacement and in less time. The New models had the most displacement and took longer to stabilize. It appears a 30-40 min warm-up was required to become reasonably stable. By that it is meant the time required for a reliable reading to be taken was passed without changes in reading of more than 1 g/m^3 or about 10 minutes.

2. A 23.1°C cold start warm-up with previous zero. The four units as describe above were again cold-started the next day, while retaining the zero position of the zero control from the previous tests. After 10 and again 32 minutes the units were all re-zeroed. After 10-18 additional minutes of stable readings, the Drierite tubes were removed, the flow slightly readjusted to 1.0 SCFH. Readings were monitored for 6 minutes during which substantial changes were noted. At that time the Drierite tubes were replaced, and readings monitored an additional 15 minutes until no changes were noted for several minutes. The results are shown in Figure 2.

The units initially read -3 to -9 g/m^3 at startup. Readings gradually drifted upwards for 30 minutes, though less so for an additional 18 minutes. Removing the Drierite tube (about 40% used) caused the Old Model to drop drastically to -13 g/m^3. The other units dropped as well by about -5, even though these units had the internal drying system. Drierite is essential in the Old Model, which was most sensitive to humidity, and probably improves stability of the newer Fumiscopes with internal drying systems. Water vapor (m.w. 18) being less dense than N_2 or air (m.w. 28) reduces air density. After reinstalling the

Drierite tubes, the units again drifted upward significantly, though the Old Model had further to recover, it also showed less drift after the initial recovery. Though difficult to quantify, it would seem good practice to avoid letting the units run without a Drierite tube attached at all times.

3. A 23.1°C cold start after 4-d unused. After allowing all units to remain unused for 4-d, the warm-up test was repeated. This test was allowed to run continually for 3.5 h without re-zeroing. The test started with units at the previous zero setting. The test was terminated after 5 hours. After 3 hours of operation, the Drierite tube was about 53% consumed (pink) and was measured every hour for consumption until the end. The data is presented in Figs. 3a, b.

At startup, the units read from -5 to -10, the Old Model again appeared less affected. Rapid increase took place over the first 15 minutes, with rate of change decreasing, but still high, over the next 30 minutes. By 60 min greater stability was achieved, and readings were taken at 5-min intervals. After 3 hours of relative stability (changes of 1 g/m^3 increments every 20-30 min) the units were re-zeroed (the Old Model was again most stable and removed for another test). After this time, the units renewed the gradual upward drift by 1 g/m^3 but still had longer periods of 10-20 minutes of no change. After about the 50-60-min mark, stable times were long enough to allow consecutive readings without re-zeroing the Fumiscope, since changes were slight, and within operating sensitivity of the units. The Old Model performed the best. Measuring the Drierite indicated no effect on the baseline zero, even though about 70% of the tubes were consumed (Figure 9).

4. A 23°C warm start with stable Old Model with increased R.H. After 4-h of continuous operation, the Old Model was connected to higher humidity source made by putting an aquarium air stone in a 2-L flask with 1.8-L of distilled water. It was not possible to accurately measure this RH. But, it will be intuitively a higher RH than room air at 45%. The Old Model was run continually for 2-h, with fresh Drierite. The consumed Drierite was estimated periodically by measuring the proportion of pink/blue 32 g Drierite tube. Since this unit was in operation 4-h previous, the warm-up drift was negligible over 2-h, shifting up 1 g/m^3 after 22 min, and remaining there for the duration. After 2-h, the Drierite was

removed and the effect noted. With this degree of stability, multiple readings can be taken without re-zero. Results are shown in Figure 5.

The condition of the Drierite indicated that in a humid environment, 40% was used, with no apparent effect on the Fumiscope. Any breakthrough or low efficiency should be indicated by a large drop from the zero, as indicated when the Drierite was removed. The effect was even less when Drierite was removed form units with internal drying, as would be expected. Still, it would be advisable to use Drierite tubes at all times. When Drierite is extensively used, the primary pink front moves roughly equally through a vertical column. There was no sharp demarcation line between pink and blue.

5. A 9.8°C cold start, only older units re-zeroed, turned off 1-day. In this test, only the Old and Old-Retro units were re-zeroed at startup, the "New" units were kept at previous zero. The units were kept overnight in a refrigerated cabinet, where all tests took place (Figure 11)

Results are shown in Figure 5. On turn-on, the older units read out deeply negative g/m^3. After 25 minutes of operation drift was surprisingly small from turn-on values, compared with the earlier tests, but still drifted upward as much as 2 g/m^3. All units were re-zeroed after 25 minutes. After this point, units remained within 1 g/m^3 of zero value. After two hours, the Ascarite was about 50% consumed, with no visible effect on operation. The units were turned off until the next test 1-Day later.

6. Repeat cold start at 9.8°C, previous zero, turned off 1-day. The 9.8°C start-up was repeated, with units left at zero from the previous 9.8°C test. Units were not re-zeroed at startup, and had fresh Drierite tubes. The result is shown in Figure 6. Units read -2 to -4 g/m^3 at startup, with immediate upward drift over the first 15-35 minutes, after which time good stability (0 to + 1 g/m^3 over 25-120 minutes) prevailed. Following this, the units were turned off and allowed to remain on the cold cabinet overnight for the next test. Drierite consumption was about 50%. However there was a secondary drying front observed, as a very pale coloration for the first two cm at the input. This is shown in Figure 10, and indicated heavy use. No "plugging" effect was seen, as the tube was easily emptied.

7. Warm-up of cold (9.8°C) units moved to 23.2°C, turned off 1-day. After overnight keeping at 9.8°C, all units were transferred to the original Lab bench set-up. This was done to simulate a Fumiscope kept in a cold room or vehicle prior to transportation to a fumigation site where the units would be used in a warm office or monitoring site. All Drierite was refreshed, the units were at the previous 9.8°C zero, and were started simultaneously. All were re-zeroed after 10 minutes of operation and run for two hours.

The result is shown in Figure 7. At startup, readings were high and increasing. After zeroing after 10 minutes, the displays continued to steeply rise in all models over 20 minutes, but with a slower rate of upward drift after 40 minutes, but which continued through 120 minutes. As before, the Old Model (lacking internal drying, but with external Drierite) was the most stable.

8. Warm up electronics 30 minute and then turn on pump (2-switch models). Figure 8. When traveling to a fumigation site, or in then office, it is possible to turn on electronics but not the pump in some models. In order to conserve Drierite, or to avoid running with depleted Drierite, three units were run for 30 min with only electronics on, then turning on the pump. Units were started from previous zero, and re-zeroed one minute after the pumps were turned on. Readings were taken each minute.

9. Supply 95% RH air to warmed-up, stable Old Model over 3.5 hours. The Old Model unit (most sensitive to humidity) was connected to a temperature control cabinet to provide continuous 23.1° air at 95% R.H. The moist air was dried with a single Drierite tube, and then passed through a ca. 1-L canning jar containing three HOBO Temperature- R.H. data loggers. The Fumiscope had been warmed up for four The Fumiscope was zeroed with room air and a fresh Drierite tube before attaching a new Drierite tube and the dry air jar. Readings were taken each minute for one h, then every five min fro an additional 2.5 h.

10. Influence of a long leads (300 ft) on zeroing and stability. The Old Model in stable operation for over 3 hours was connected to fresh Drierite and zeroed. After operation for 5 minutes, a 300 ft section of tubing was alternately added and removed at 5-min intervals. The result is shown in Figure 10. Adding the tubing caused the zero to increase by 1 g/m^3.

After 25 minutes of operation without re-zeroing, the unit may have drifted upwards by 1 g/m^3 over two minutes, as was previously seen during extended operation.

Part 2. Tests with methyl bromide and long leads.

11. Performance of Fumiscope with short or long leads and Methyl Bromide.

The Fumiscopes are normally calibrated with a gas sample of known MeBr density (56 g/m^3). Previous findings have shown the instrument to be linear over a wide range to well over 200 g/m^3, the highest dose tested, with no apparent drop-off in sensitivity. The source of the calibration gas is a gas bag attached to the Fumiscope with a short lead of less than few feet, and in the case of older instruments, with Drierite desiccant in the sample stream.

The Old Model Fumiscope was supplied arranged so that, by the use of a 3-way valve, the sample source could be switched to a Drierite 26930 tube and 300 ft of 0.25 O.D. LDPE sample lead connected to a Tedlar gas bag containing 80-L of about ≥80 g/m^3 MeBr. The valve could then divert the source gas to a fresh Drierite tube that was never in contact with MeBr, so the Fumiscope could be re-zeroed if desired with uncontaminated air (Figure 21).

In the first test the Fumiscope was connected to the gas bag through fresh Drierite and 300' of tubing that was previously used with MeBr, but air-flushed for several minutes. After 10 minutes of stable high readings the gas was disconnected, the tube and Drierite flushed, and then re-zeroed with the used Drierite. A second run was made by first re-zeroing with fresh Drierite, then reconnecting through the used Drierite, the tubing, and the gas bag. The instrument was zeroed with uncontaminated, fresh Drierite. The test was allowed to run for about 25 minutes before the instrument was disconnected form the gas and zeroed with fresh Drierite.

Finally, the Fumiscope was re-zeroed with fresh Drierite and then connected directly to the gas source and run for about 15 minutes until a stable reading was obtained for five minutes. The results are shown in Figure 11-a. All sequential test runs had time adjusted to a common start time.

The first Fumiscope run reached a high of 77 g/m^3 after about 20 minutes. The increase was gradual, but was delayed by about four minutes, because the volume of the clean tubing was about 1660 ml, the flow rate was about 444 ml/min, and thus it actually took about 15 minutes of gas flow to reach the terminal reading. The Fumiscope took four minutes to reach zero after disconnecting the gas source. A second run showed an immediate increase after connection to the used Drierite and gas supply. This was the apparently the result of residual MeBr degassing form the Drierite. After four minutes, fresh gas entered the Fumiscope and readings climbed to a stable 80 g/m^3 after another 20 minutes. The Fumiscope responded faster and to a higher reading the second run. This could be due to the adsorption and possible absorption of MeBr by the system during the first run. During the second run, the instrument was switched to the fresh Drierite for zeroing, where it only took 1.5 minutes to reach zero. Clearly, zeroing through used Drierite took a much longer time. This may lead to prematurely setting a false baseline zero if the operator does not wait a sufficient time to re-zero.

A third run was made from a clean zero with fresh Drierite, and the gas bag connected without the 300 ft of tubing. This direct connection resulted in a very fast response, reaching a higher maximum of ≥80 g/m^3 in less than three minutes. The Fumiscope drifted slightly higher (2 g) over the next 15 minutes. Clearly, the Fumiscope read higher when connected directly as opposed to through 300 ft of tubing.

As a means of comparison (Figure 11-b) to the second Fumiscope run, the gas sample was connected to a Spectros IR monitor through the 300 ft of flushed tubing and then again directly to the gas source. Through the tubing it took about 1.5 minutes for the first MeBr to enter. The Spectros was configured for a 20 second purge IR cell purge cycle followed by a one minute measure cycle. Therefore the readings occurred in steps of one minute cycles. Again, the readings were low until a large volume of gas passed through the tubing. Directly connecting the Spectros to the gas bag resulted in an immediate increase to 85 g/m^3. Again, the reading with tubing was lower than that with no tubing. Figure 12 directly compares the second run of the Fumiscope with Spectros runs with and without tubing. The direct sample readings of the Fumiscope and Spectros were 83 and 85 g/m^3 respectively. This was likely a calibration, sensitivity and zeroing issue, as a post-test calibration of the

Fumiscope needed a 1 g/m^3 upward adjustment, thus placing the units within 1 g/m^3 with the same gas supply for the maximum readings measured.

The flow rate of the Spectros was measured at 1072 ml/min. with tubing, and 1502 ml/min without. The vacuum needed to draw a sample was measured at -11.33 mm Hg with the Fumiscope and -12.04 mm Hg with the Spectros.

12. Performance of Spectros and Fumiscope with sequential samples. The result of 12 above, suggest that sorption is an issue with long sample tubes. Another possibility is that reduced pressure caused by the internal vacuum pump resulted in lower pressure, hence lower gas density. However, the Spectros has internal operating software to calculate pressure compensation.

The next tests were conducted by running three consecutive sample runs with the Spectros and Fumiscope, each run comprised of a run with 300 ft of sample tube, clean re-zeroing, and followed by a run with direct gas-bag-to-instrument gas supply. The only difference was that the Fumiscope required the use of the Drierite tube. The results are shown in figs. 12-a, 12–b.

The first run with the Spectros (Fig. 12-a) used clean, flushed tubing. It can be seen that there was a considerably lower reading in the first run, compared with a direct sample. The difference lessened with the second and third consecutive runs, but still existed.

The first run with the Fumiscope was done with un-flushed sample tube. There was an initial run-up, followed by a temporary plateau, then continuation to the termination. This suggests that during the time delay between the Spectros test and the Fumiscope test, the MeBr within the sample line had somehow decreased. The first direct run achieved a high reading after about 4 minutes. The second run with tubing was done with flushed tubing. It took four minutes for the gas to reach the Fumiscope, but there were readings of 2 g/m^3 picked up from the used Drierite. Again, the direct run was significantly higher. The third run was made with clean re-zeroing, but the air flow was inadvertently left at the lower power used in the previous direct gas run. The air flow would decrease from 1.0 to 0.5 SCFH the tube were attached, and pump flow needed to be increased to keep flows at the standard 1.0 SCFH. This had made no difference in the outcome of the third run, as the

MeBr reading increased slightly (due to less sorption?) but the direct sample still remained higher.

13. Collection of exhaust gas to cross-check lower levels. It was speculated that if the exhaust gas could be collected and re-fed to the instruments, we could see that the decrease was not due to vacuum influences, but to MeBr lost to sorption of dissipation through the tube wall. To test this, we collected, in a 3-L Tedlar bag, the exhaust from both instruments during a terminal period of stability when both units were at maximum readout for the three sequential replicates as described in **12 (**above) both with 300 ft of tube and again direct into the instrument. The readout from the immediate reinfusion of the collected gas was time-adjusted so as to appear simultaneous with the original reading. The results for the Spectros and Fumiscope are shown in Figs. 13-a, 13-b, respectively.

The first Spectros (13-a) run was with a clean, flushed sample line and fresh Drierite. Re-infused gas read lower than the original. If the first observed discrepancies were due to pressure changes, we would have expected readings of $\geq$80 g/m^3 or above. This was not the case. The direct input reading and collection for the Spectros also had a first low replicate, due to the fresh Drierite, though readings increased after multiple runs, but still were different. This suggests sorption has decreased during conditioning of the sample tube.

With the Fumiscope (13-b), the result was similar. The tube was not flushed for the first replicate, and this showed as an early plateau in the reading. This would indicate that during set-up time, the tube lost MeBr. The second replicate had initial low readings due to degassing form the contaminated Drierite, again pointing to the need for fresh Drierite during re-zeroing. A short plateau for the third replicate was described above (12.) caused by failure to increase air flow between previous direct reading after adding the 300 ft of tubing. This was remedied and the replicate continued with no obvious fault, since recovery during the peak was the objective.

Subsequent replicates had higher readings, but the discrepancy did not disappear. Gas loss from the tubing due to sorption (both adsorption and possibly absorption) is the probable cause.

Conclusions and Recommendations.

1. All units tested required warm-up times longer than 10 minutes to reach good stability. Good stability should be defined as a stable zero with drift not to exceed 1 g/m^3 over an arbitrary period, perhaps 10 minutes. This allows a useful reading to be taken without introducing a false baseline zero. Warm-up may be as long as ½ hour.

2. The use of Drierite should be mandatory at all times. Units should not be run without Drierite. It might be prudent to store the Fumiscopes with one fresh (mostly blue) Drierite tube attached and connected at both input in exit. It would be recommended avoid large temperature differences between storage and use at a fumigation site.

3. The 15-cm Drierite tubes (Hammond #26930) have a long life and can be used until at least ¾ used up. There was no indication of failure to that point.

4. It is possible to reduce pre-use warm-up time if units with dual switching can be warmed up in the meter mode for a half hour before using the pump, which then requires an additional 10 minute after the pump is turned on.

5. There is a conditioning period required when using fresh Drierite as the readings will be lower until the Drierite has fully absorbed the sample MeBr. Corollary to this, Drierite degasses when no gas source is connected.

6. Due to 5 (above) it is essential that Fumiscopes be zeroed with fresh Drierite not exposed to MeBr. Unused Drierite zeros much faster. To not do this requires a much longer zeroing time, and may lead to setting a false lower baseline if adequate time is not allowed. This also slows the entire process of getting timely readings.

7. Adding a significant amount of tubing (here 300 ft) after zeroing may change the zero upward, when reconnecting to sample lines, though the change was 1 g/m^3, longer leads might have greater effect.

8. The initial use of sample leads (and Drierite) not fully sorbed with MeBr will result in low readings. This may take a long time to come to equilibrium. It is essential to purge long leads continually, and not allow leads to remain idle while monitoring multiple leads if timely readings are needed.

9. The problems with long leads applies to both the Fumiscope and Spectros monitors, though much less so than with the Spectros, due to its much faster flow rates.

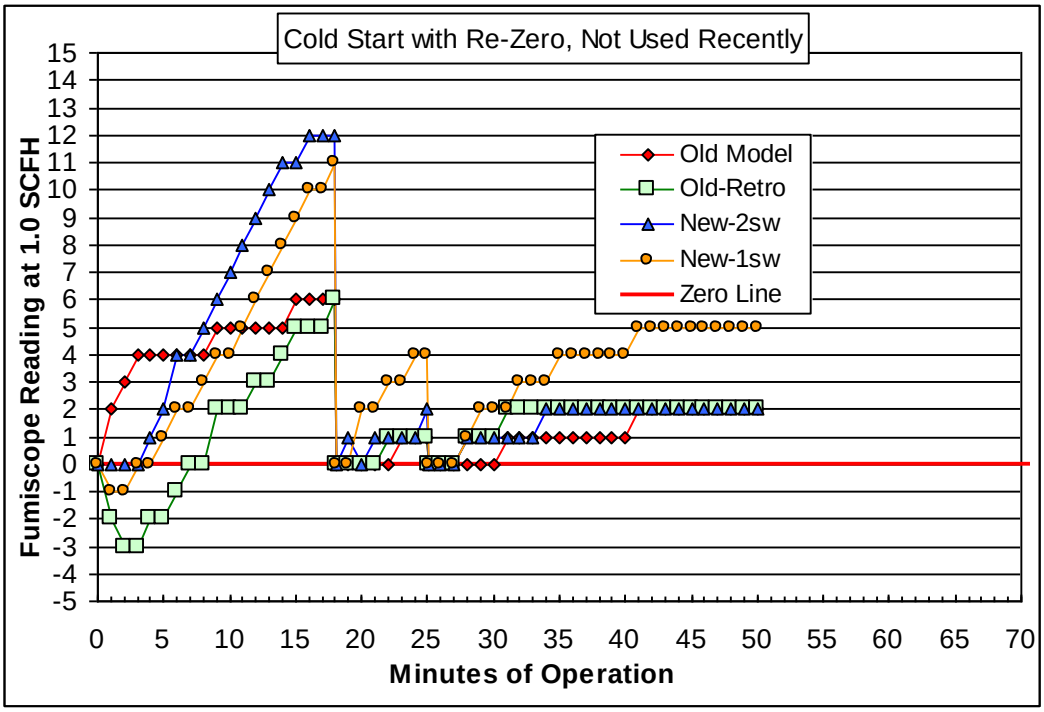


Figure 1. Warm-up of four Fumiscope variants at 23.1°C after a long period of non-use. Instruments were re-zeroed at start-up and after 18 minutes. Drift was observed over 70 minutes.

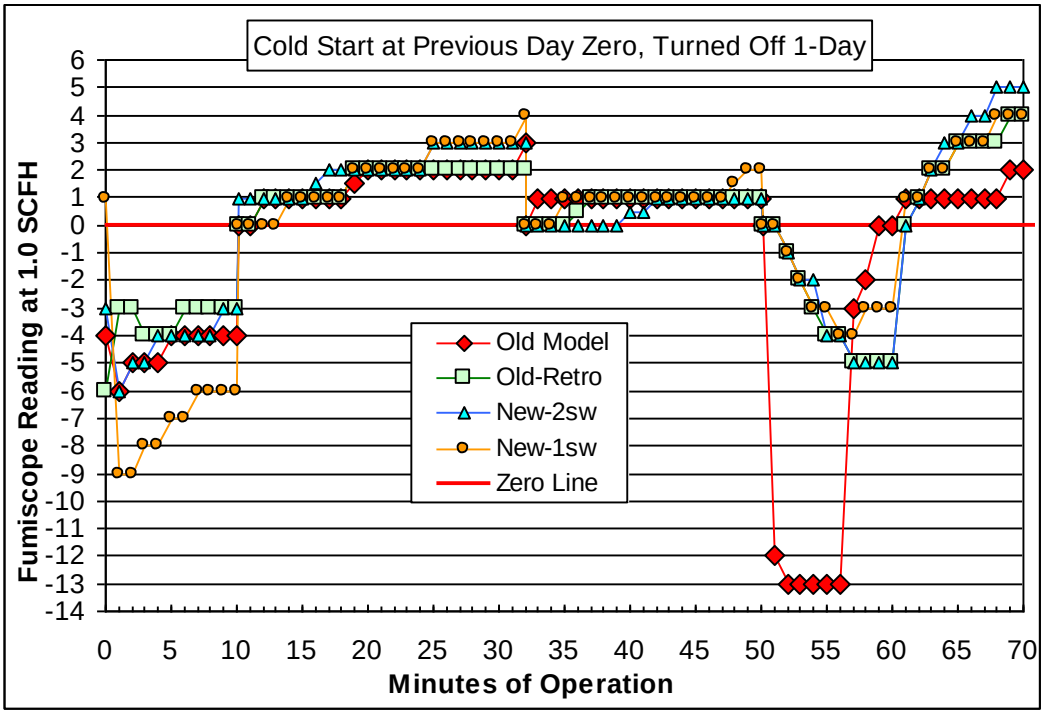


Figure 2. Warm-up of four Fumiscope variants on day after previous use and zeroing. Units were re-zeroed after 10 minutes. The Drierite was removed and replaced after 50 minutes.

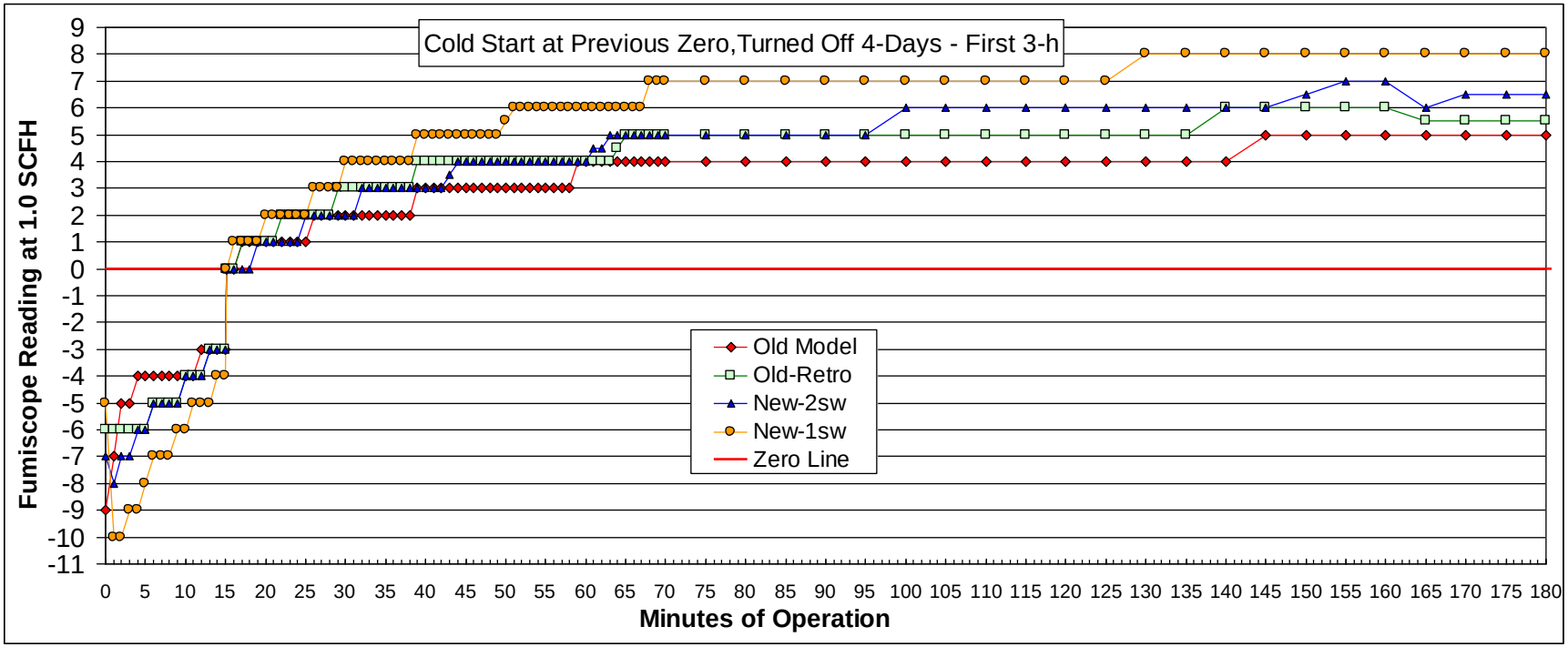


Figure 3-a. Warm-up of four Fumiscope variants after four days of non-use and storage at 23.1°C ambient. All were connected to the in-line Hammond #26930, 32 g, 10-20 mesh Drierite tube. Units were turned on with zero in previous position. After 10 minutes, they were simultaneously re-zeroed. Drift was monitored every minute for 70 minutes, and thereafter every five minutes.

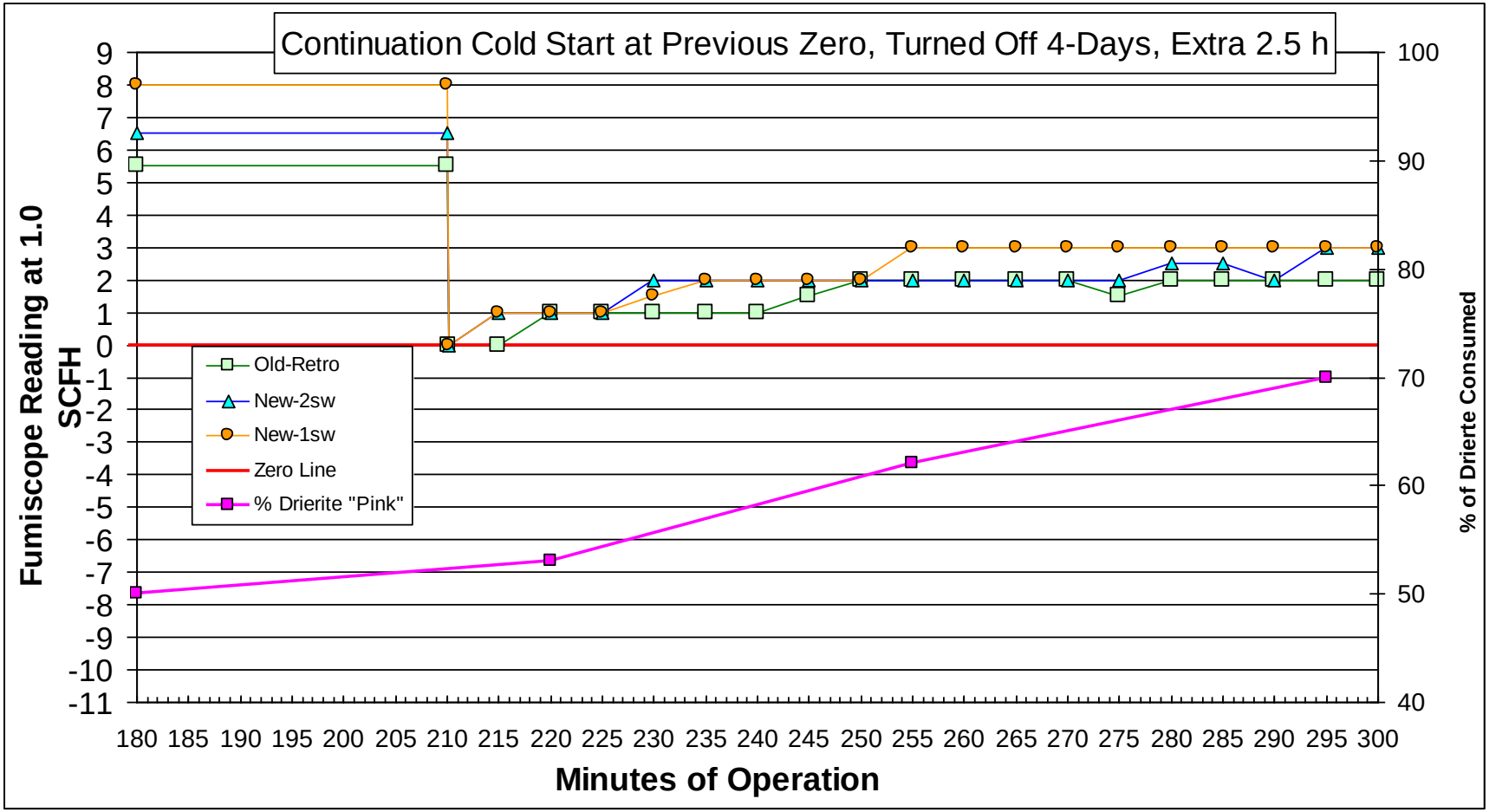


Figure 3-b. Continuation for two additional hours of warm-up of three Fumiscopes from figure 3a. After three hours of operation, the Drierite was measured and used proportion estimated. Instruments were re-zeroed again after 3.5 h to observe additional drift and Drierite consumption. The Old Model was further tested individually in another test, as it was the most stable and did not have internal drying system of the other variants.

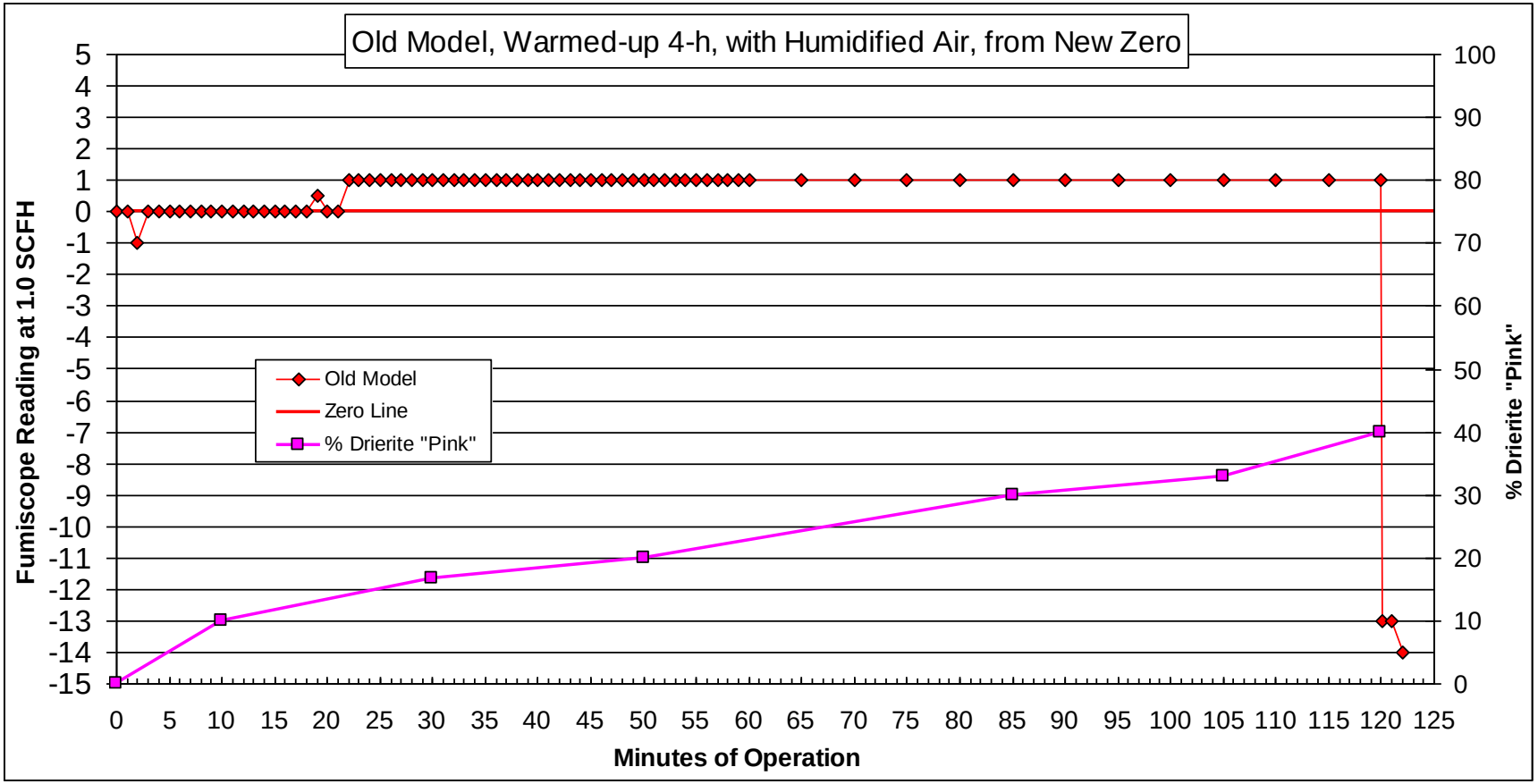


Figure 4. The Old Model was allowed to run an additional two hours after a 4-h warm-up. Stability was excellent. Drierite consumption was consistent, and had no apparent effect on operation. Removal of the Drierite tube after 120 minutes illustrates effect of less dense, moist air on operation of the Old Model, which lacks internal drying system. This model was consistently most stable.

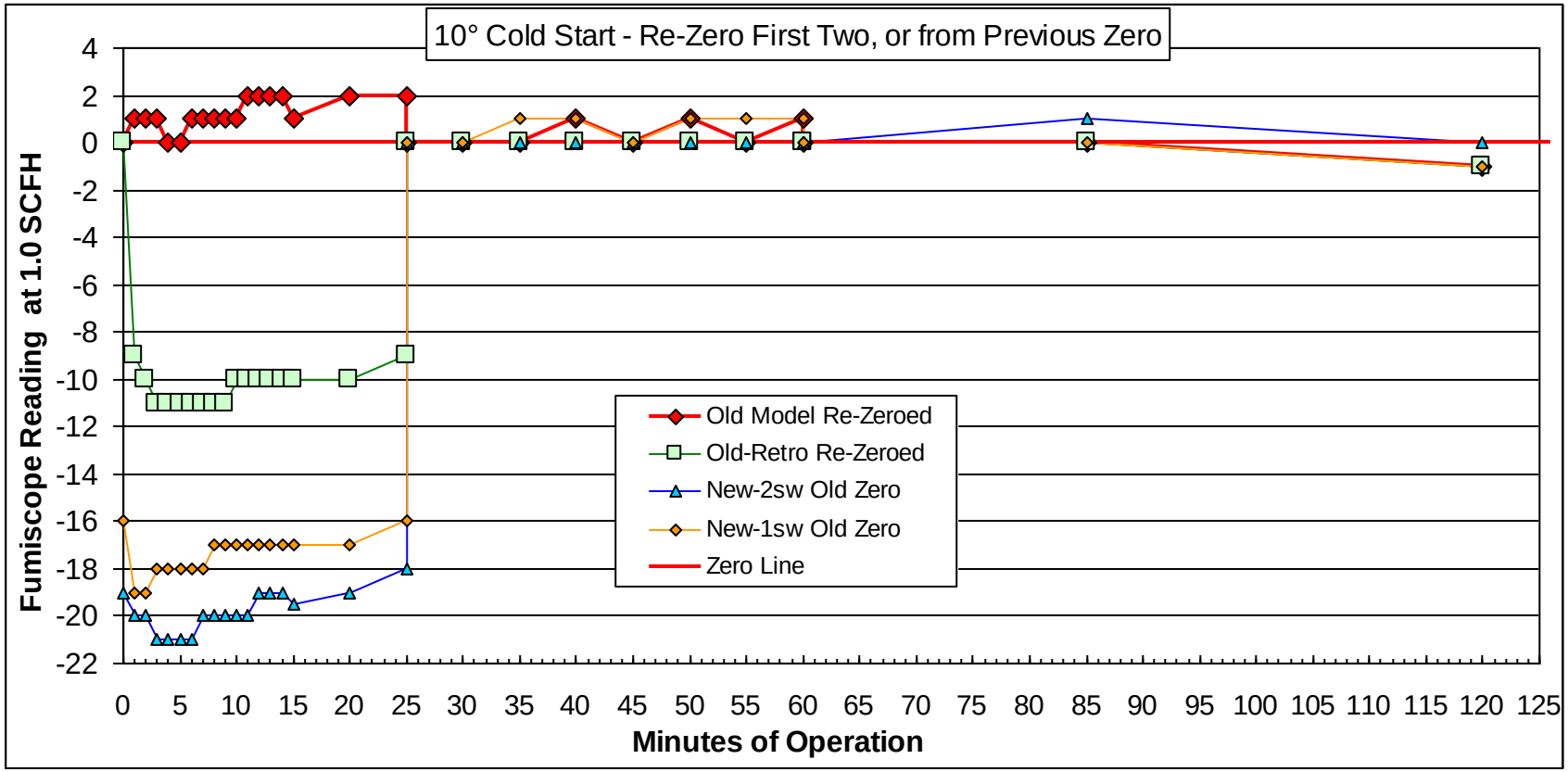


Figure 5. Warm-up of four Fumiscope variants after overnight chilling to 9.8°C. The Old Model and Old-Retro models were zeroed on start-up. All units were re-zeroed after 25 minutes. The newer units with built-in drying system had the most drift at start-up. Stability was better after 25 minutes, after which time drift was ±1 g/m^3 on display. At start, the zero was in the position of previous test at 23.1°C.

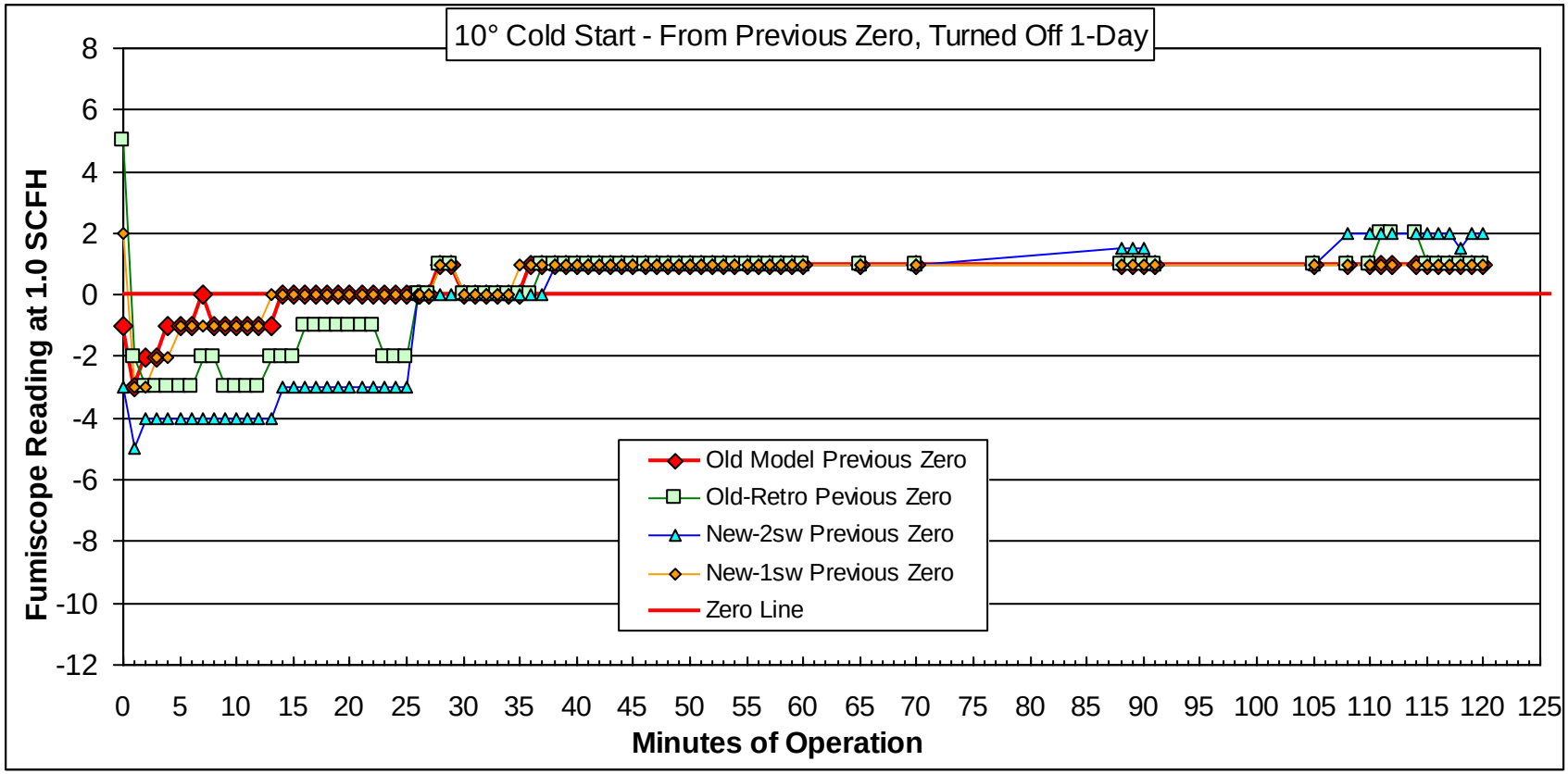


Figure 6. Warm-up of four Fumiscope variants after an additional day at 9.8°C. Units were at the zero of the previous cold test, and were cold started. Drift was evident and stability improved after about 15-25 minutes, after which time drift was within + 1.0 g/m^3.

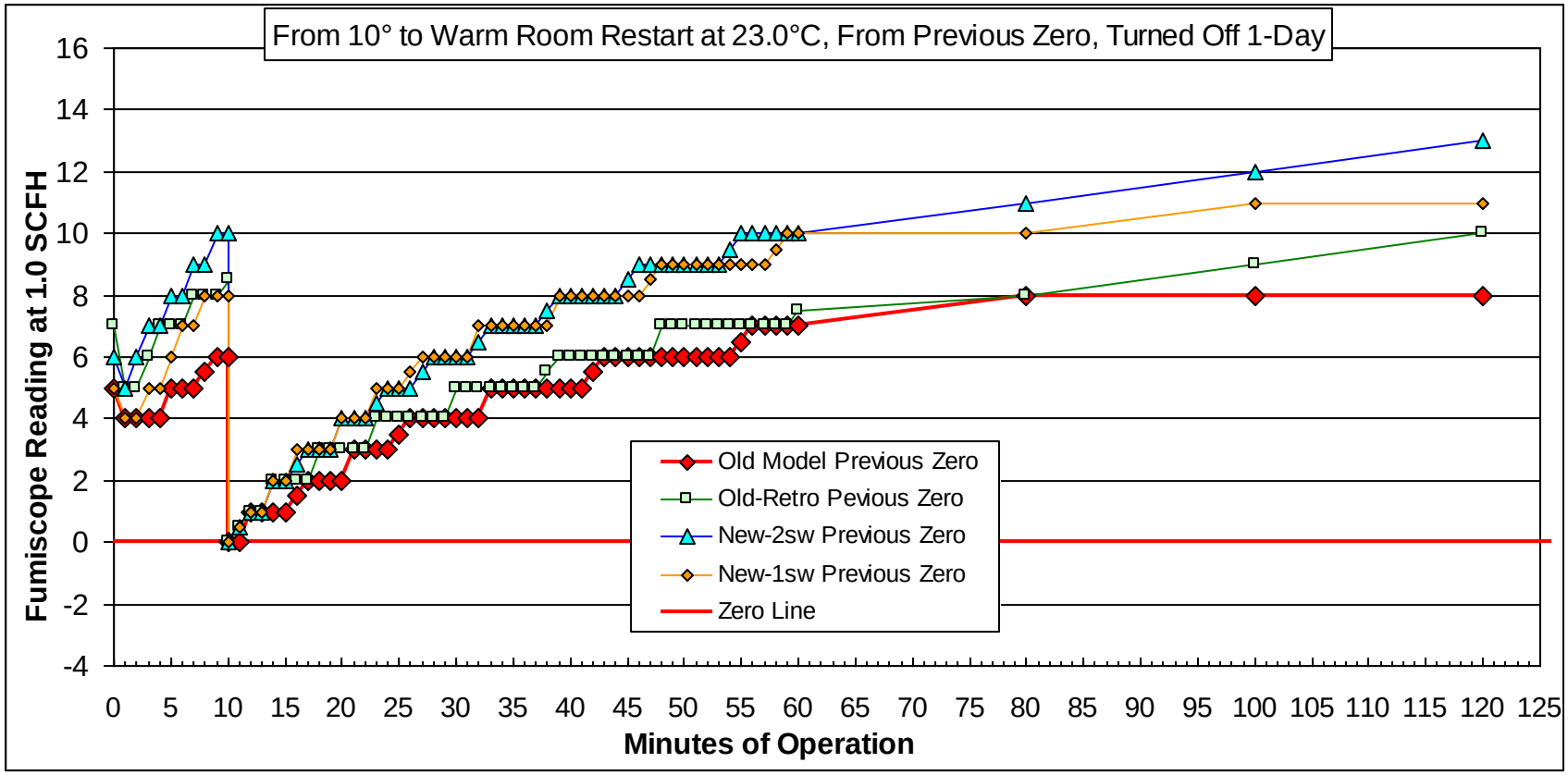


Figure 7. Warm-up of four Fumiscope variants after being held unused in cold storage overnight. Units were moved to Lab. Temperature of 23.1°C to start this test. This was to simulate a cold unit being moved to a warm area just before use. Start-up was with previous zero, and had large drift. After zeroing after 10 minutes, the displays continued to rise in all models over 20 minutes, but with a slower rate of upward later, but which continued through 120 minutes. As before, the Old Model (lacking internal drying, but with external Drierite) was the most stable.

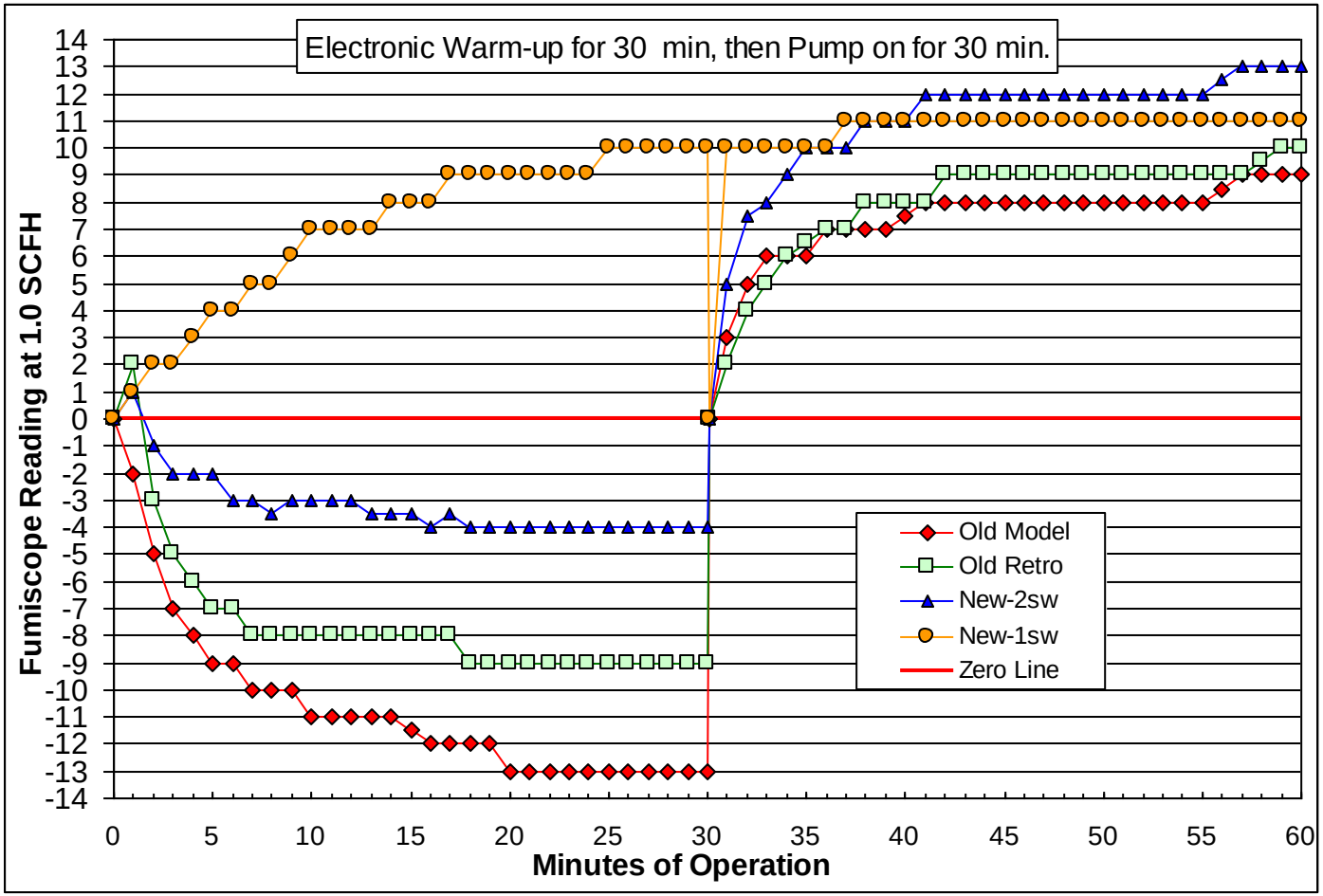


Figure 8. Fumiscopes electronics were warmed up with pumps off for 30 min. (except New-1sw model), re-zeroed, then pumps were turned on after 30 min. Test began with all Fumiscopes at previous zero. The New-1sw was on from start. With 2-switch models, relative stability was obtained about 10 minutes after pump was turned on, but after electronics 30 minutes warm-up.

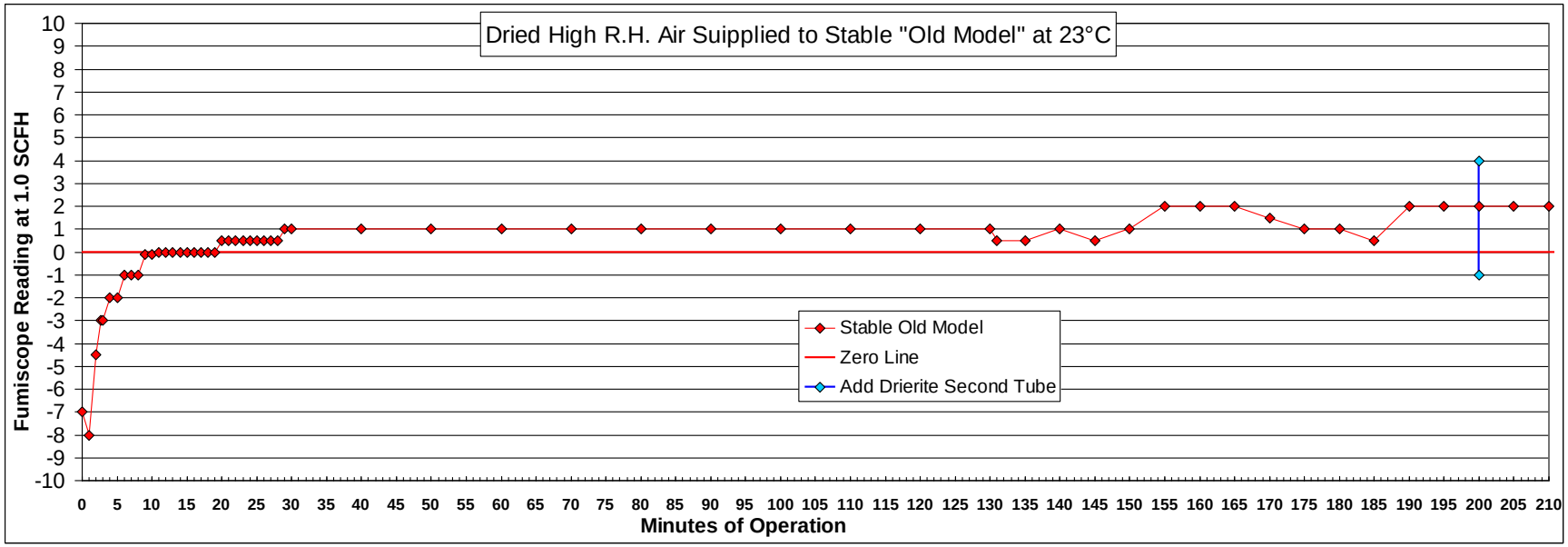


Figure 9. Continuous running of a stable, Old Model Fumiscope with source air at 95% R.H. and 23.1°C. The sample passed through a Hammond 26930 Drierite tube, then into a 0.95-L in-line drying jar with three HOBO data loggers. After the internal moisture was purged (by 10 minutes), the readings were unchanged after ½ of the Drierite tube was consumed. Addition of a second Drierite tube after 200 minutes resulted in no change in zero for 10 minutes. All data loggers bottomed at the minimum range of the data logger (23.5%). A brief period of ±1 g/m^3 baseline may be the result of circuit voltage fluctuations during the test.

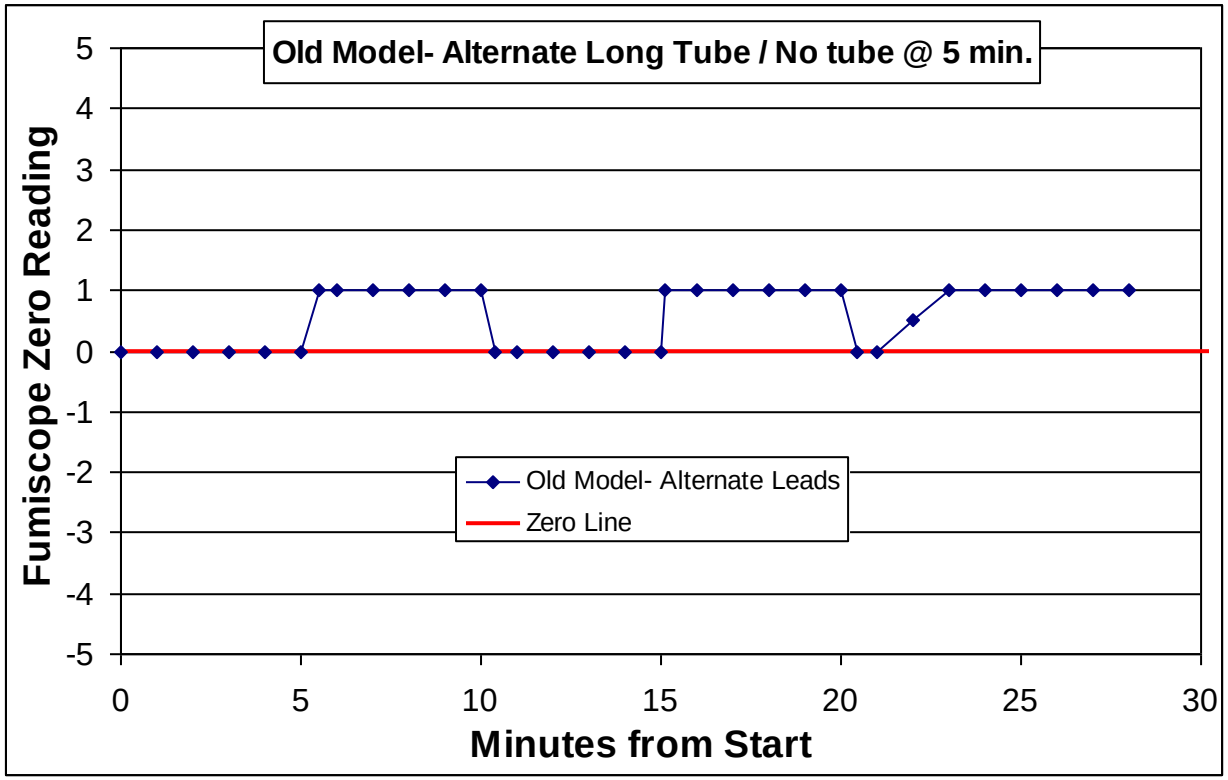


Figure 10. A warmed-up, stable Old Model Fumiscope was zeroed for five minutes with only Drierite tube attached, then 300 ft of LDPE 0.25 inch O.D. sample line was attached and removed at 5-min intervals. The result was a small but identifiable change in zero. After over 20 minutes, drift may have influenced the zero reading.

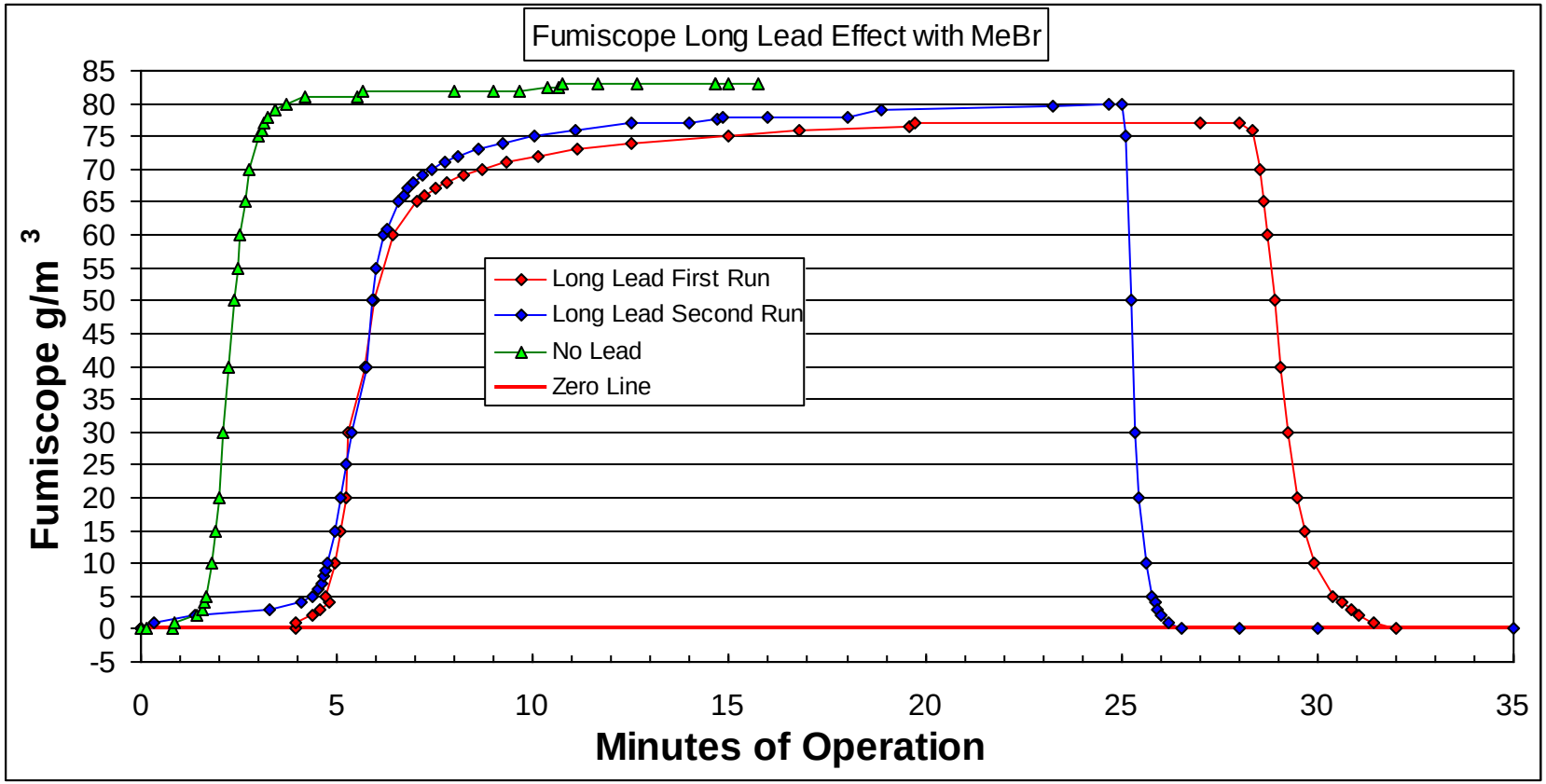


Figure 11-a. Time required for two sequential Fumiscope readings of MeBr with a 300 ft sample line compared with direct connection to the Fumiscope. The first run of the Fumiscope used flushed sample tube and fresh Drierite. The second run illustrated the residual effect from used Drierite.

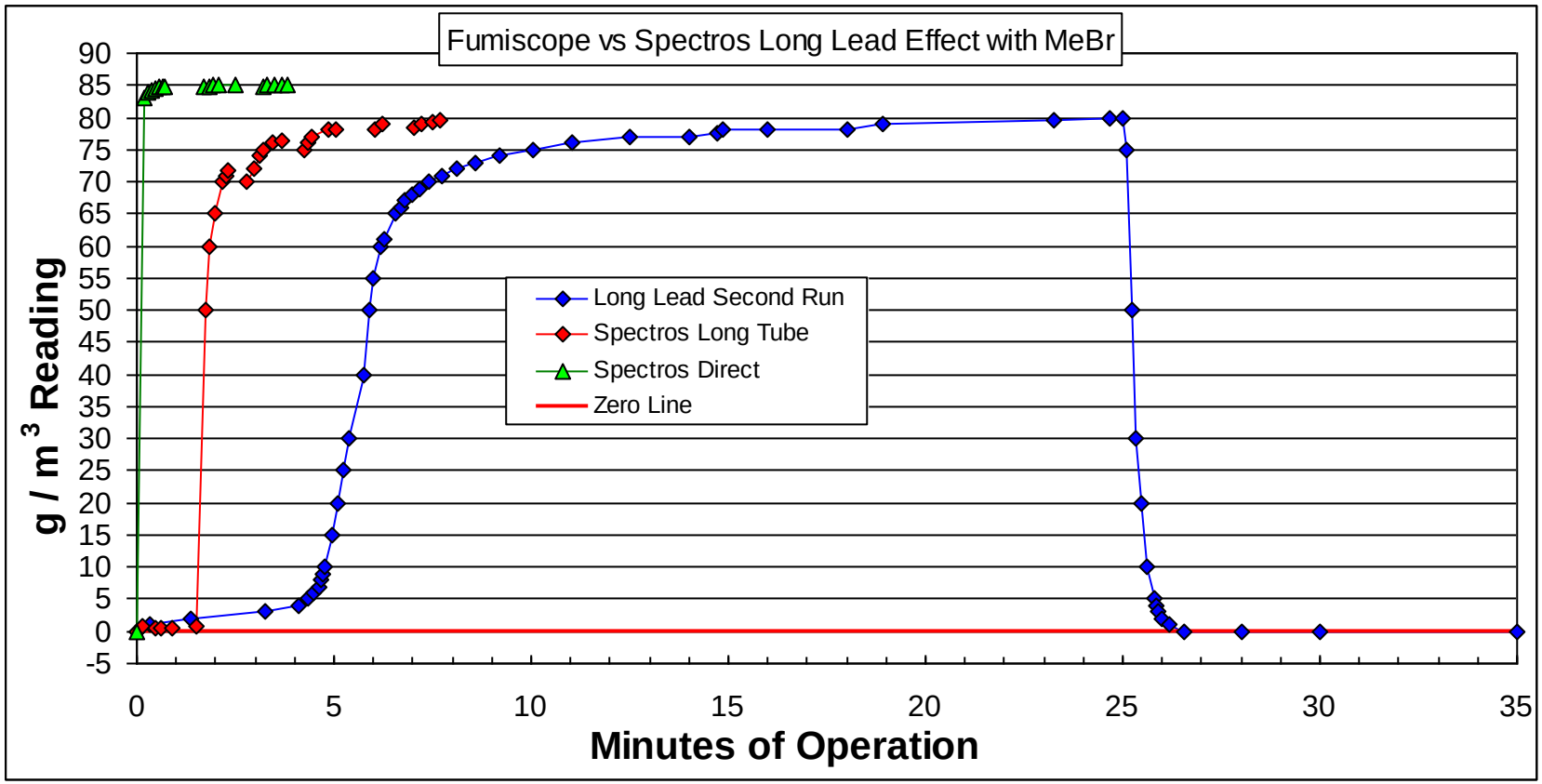


Figure 11-b. Time required for readings of MeBr with a 300 ft sample line (run two form previous Figure 11-a) compared with a Spectros unit and direct connection of a Spectros unit to the same MeBr source. The configuration of this Spectros is for a 20 second cell purge followed by a one minute measure cycle.

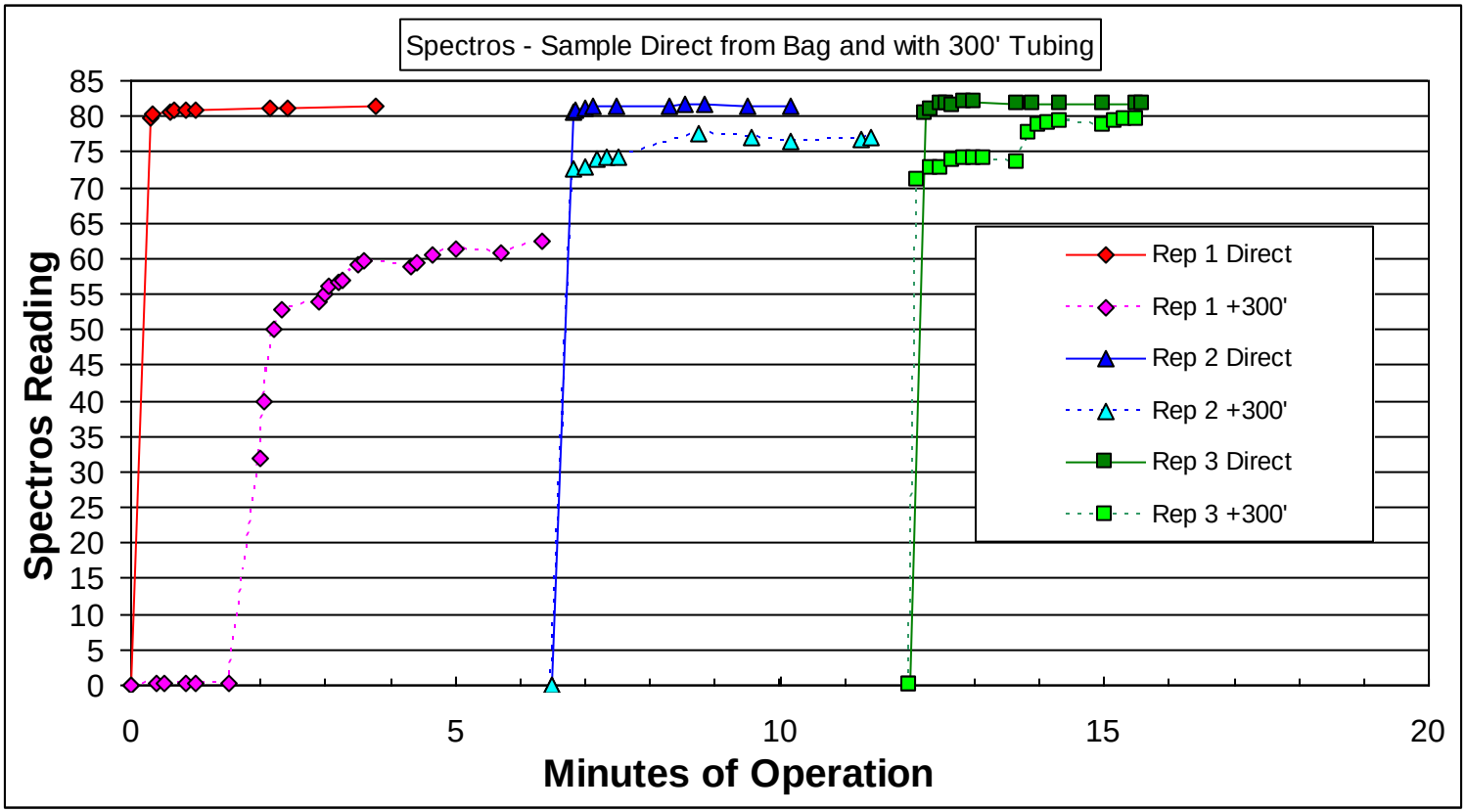


Figure 12-a. Comparison of sequential readings with either a 300 ft tube to gas source, or directly connecting to the Spectros. The initial run (with 300 ft of tube) was with flushed tube, therefore a 1.5 minute lag was noted.

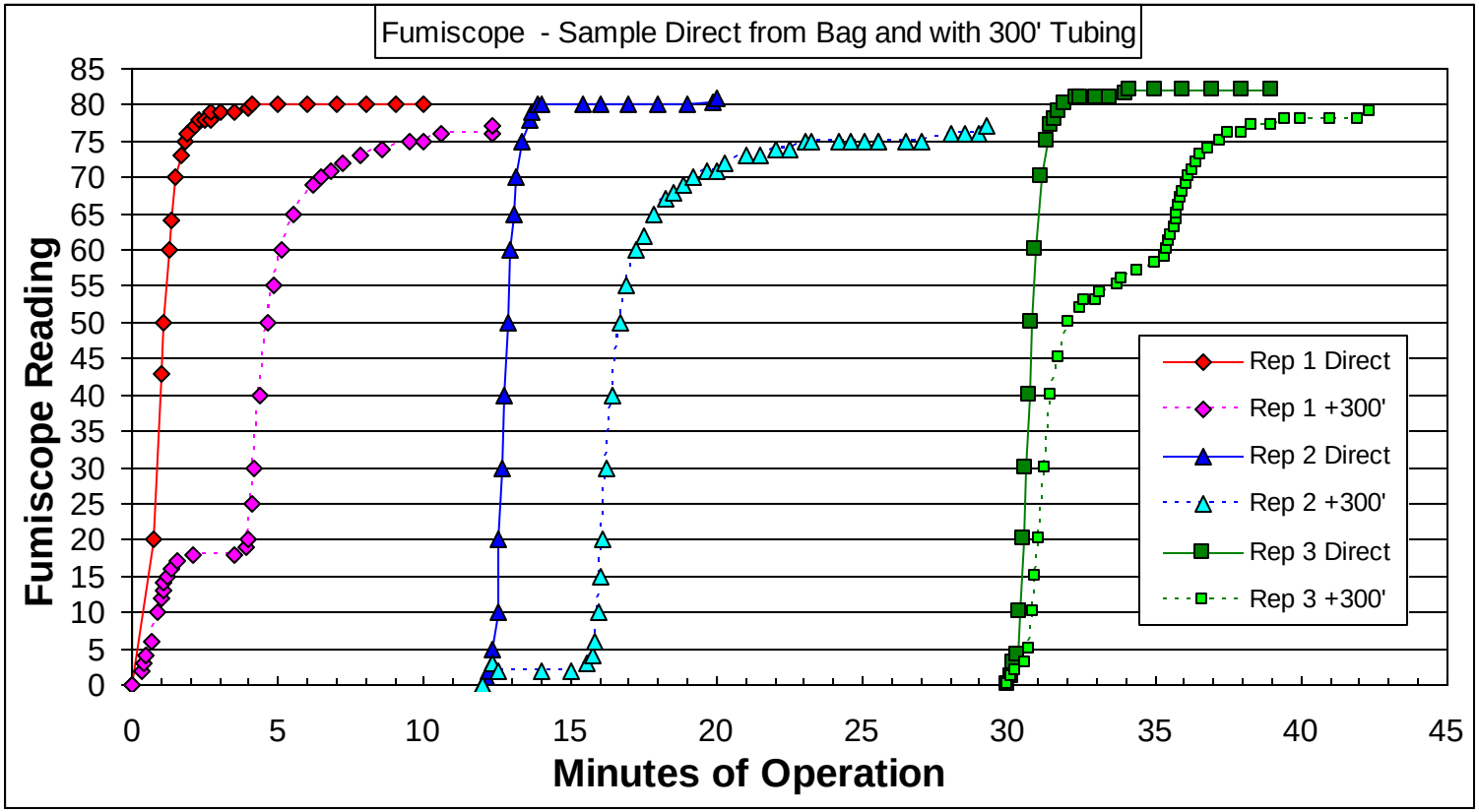
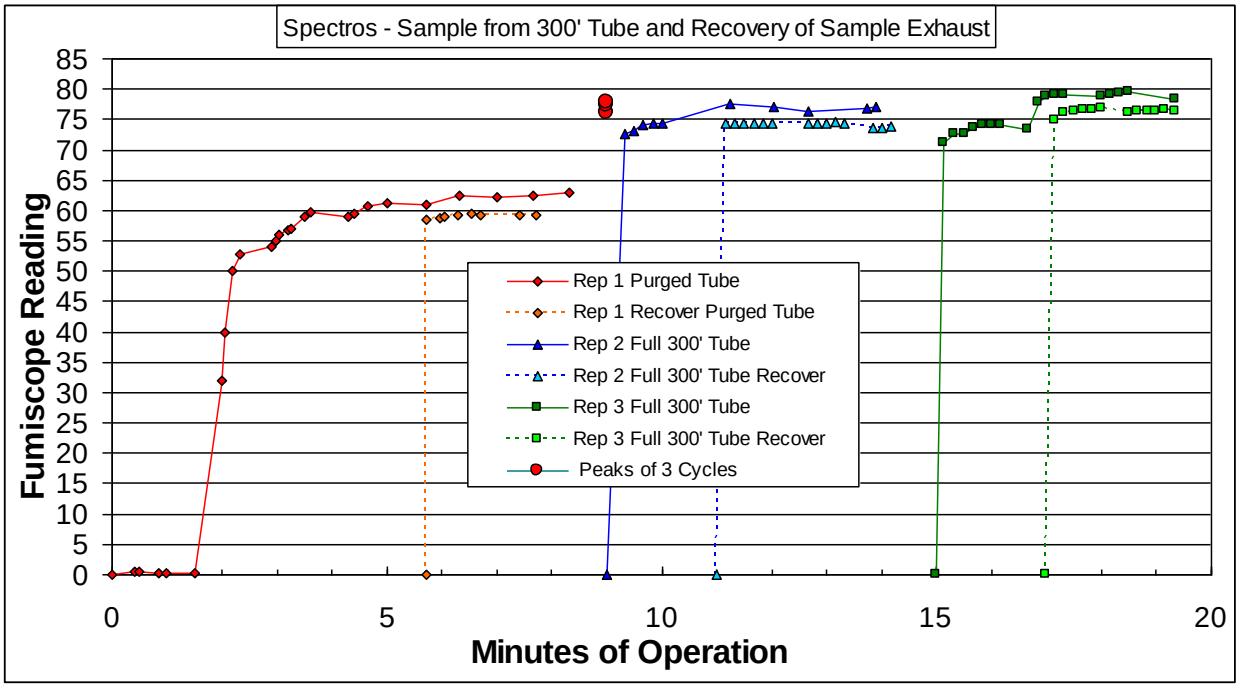


Figure 12-b. Comparison of paired, sequential readings with either a 300 ft tube to gas source, or directly connecting to the Fumiscope. The initial run (with 300 ft of tube) was with an un-purged flushed tube, therefore response was quick, but a plateau was noted due to loss of gas from the tube during operating with a direct connection.



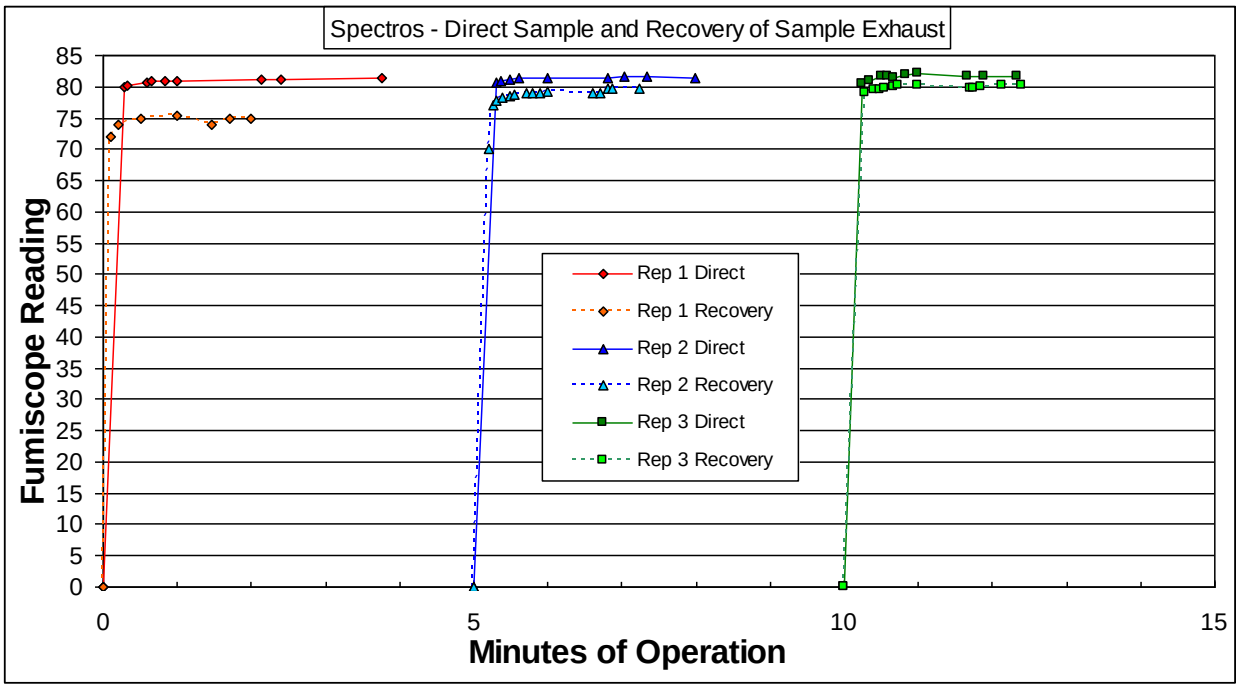
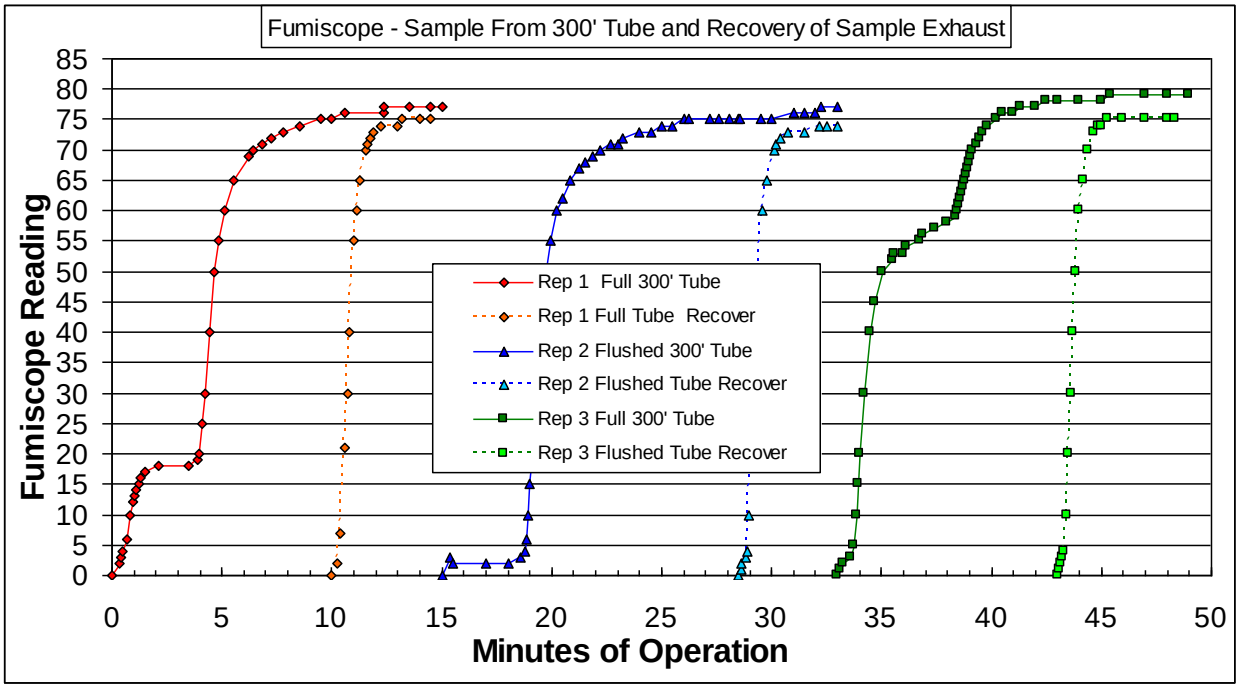


Figure 13-a. Recovery and re-test of MeBr samples by the Spectros IR analyzer with or without 300 ft of tube attached.



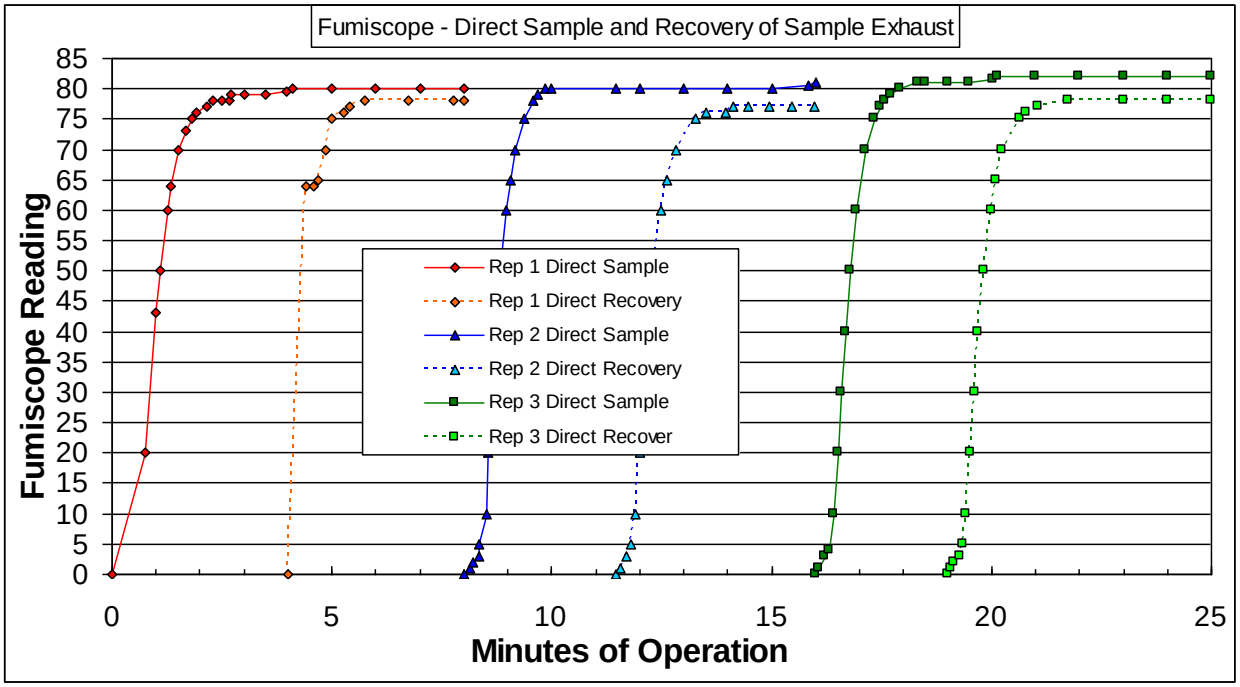


Figure 13-b. Recovery and re-test of MeBr samples by the Old Model Fumiscope with or without 300 ft of tube attached.

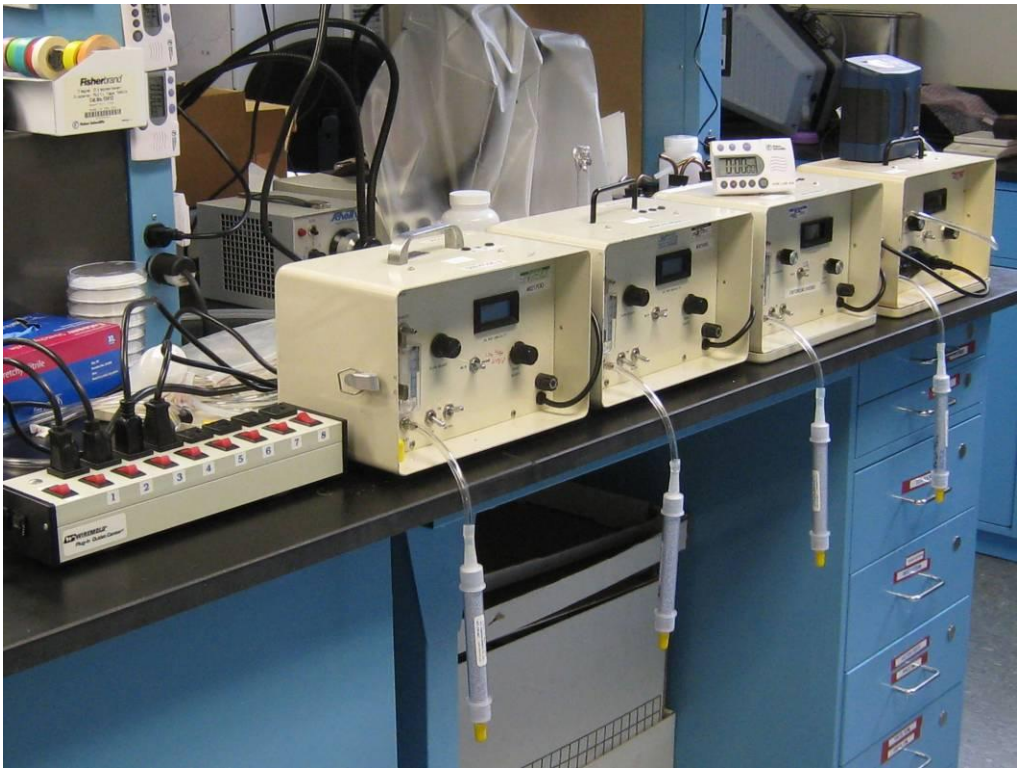


Figure 14. Lab Set-up of four Fumiscopes with attached Drierite tubes.

Figure 15. Condition of the four Drierite tubes from Test 4, after 5 hours of continuous operation at Lab RH of 45.1%. Average consumption was estimated to be about 70% of 32 g.

Figure 16. Zones of drying in a 15-cm Drierite 26930 tube after hours of continuous use. Five zones are observed from right: 1. 50% unused, 2. fine dark purple primary active front, 3. light purple band, 4. pink band of depleted Drierite, 5. finally white, completely exhausted Drierite. With this degree of use, there was no apparent effect on Fumiscope zeros, as all continued to operate with little drift after warm-up.

Figure 17. Fumiscopes in operation within refrigerated cabinet at 9.8°C

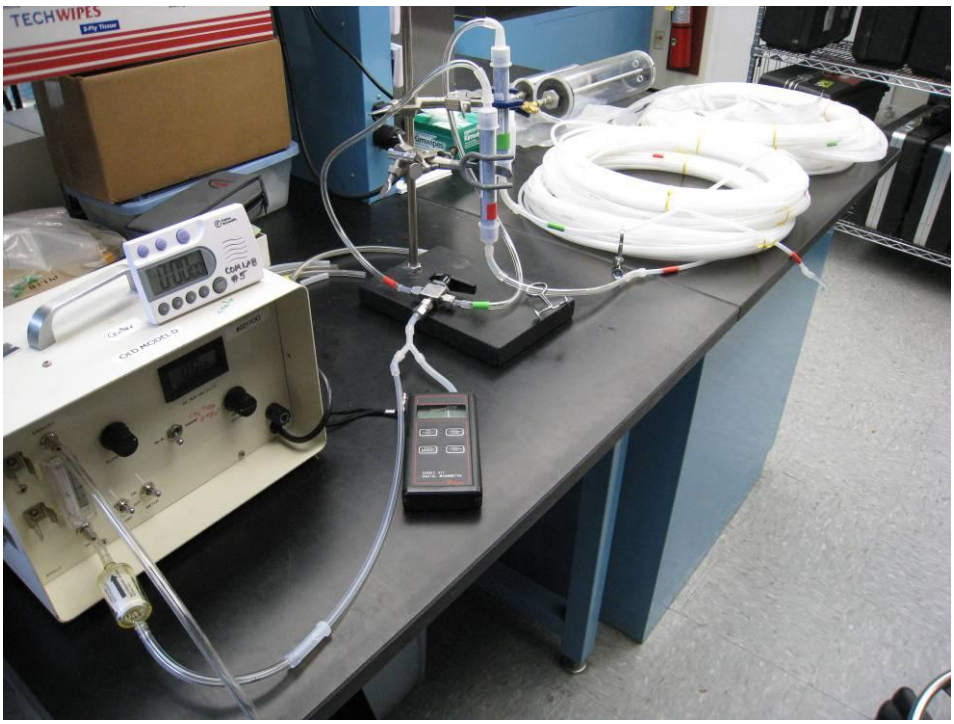


Figure 18. Fumiscope with option to instantly switch between used Drierite and 300-ft sample line and fresh, uncontaminated Drierite or virgin 300-ft sample tube.

Technical Report: Zeroing methods for the Fumiscope.

Alan V. Barak

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Background

The Fumiscope, a thermal conductivity instrument, is used by APHIS for monitoring fumigant gasses, primarily methyl bromide (MeBr). Older versions were supplied with glass tubes to hold about 10 g of 8-10 mesh indicating Drierite desiccant to dry the sample stream to a uniform and repeatable level to avoid errors. Later versions of the Fumiscope were equipped with an internal drying system, but it was found that the use of a Drierite tube improved consistent performance. APHIS requires the use of drying tubes with the Fumiscope at all times. Either the traditional Fumiscope (about 10 g) glass tube or a commercial tube containing ca. 30g of 10-20 mesh indicating Drierite is allowed. The effect of using fresh uncontaminated Drierite to achieve a new zero is unknown. Carbon dioxide (CO_2) may be present in concentrations high enough to influence Fumiscope readings; therefore an in-line CO_2 scrubber such as Ascarite may be required. The glass tube holds about 10 g of Ascarite II. It is unknown if the use of Ascarite in-line with the sample or zero air will significantly influence the zeroing process. The following tests compare: 1) The re-zeroing speed and efficiency when sample air is allowed to flow through used, MeBr-contaminated vs. clean Drierite by diverting fresh air through fresh unused Drierite via a 3-way valve, and 2) The effect of Ascarite on the zeroing process, with ambient and 1.0% v/v CO_2.

Procedures.

Calibration gas of 21,050 ppm ± 1.0% MeBr (ca. 79-81 g/m^3 at Lab variable pressure and temperature) was used in some tests (Scott-Marrin, Riverside, CA). For some tests, an 80 g/m^3 mixture of MeBr in air was prepared in 40-liter SKC Tedlar® gas bags (SKC, Inc. Eighty Four, PA). An additional mixture of 80 g/m^3 MeBr +.0% v/v CO_2 was prepared. A Fumiscope, retro-fitted with the internal drying system (Key Chemical and Equipment, Clearwater, FL) was first calibrated at 81 g/m3, based on the supplied calibration gas ppm and the existent ambient pressure and temperature. The Fumiscope was set up to allow the gas source to enter the Fumiscope through desiccant or sorbent tubes configured as to allow the supply source to be switched alternatively from two different sample sources by use of a No. B-43XS4 3-way high pressure ball valve (Swagelok, Solon OH). Drierite tubes employed were either the traditional glass tube previously supplied with some Fumiscope models utilizing ca. 10 g, 8- mesh indicating Drierite, or a purchased, #26930 disposable tube (Hammond Drierite Company, Xenia OH) using ca. 30 g of the finer 10-20 mesh Drierite. Fumiscope exhaust was monitored by a Defender 510-M Dry-Cal flow calibrator (Bios International Corp., Butler, NJ). The Fumiscope flow gauge was adjusted

to supply input MeBr at ca. 472 ± 5 ml/min (1.0 SCFH). Flow rates after disconnection of MeBr or diverted air were not re- adjusted further. Flow rates during re-zeroing were only slightly higher (ca. 480 ml/min). The experimental apparatus is shown in Figure 1a.

Tube connections were made using the 3-way brass valve previously described. The valve was fitted with three 0.25 inch compression fittings. This fitting allows direct permanent connection of the standard 0.25 inch LDPE sample lines. More flexible 0.25 in. OD, 3/16 inch ID Tygon type tube was used to facilitate connections. Connections of different size tube were accomplished by using 0.25 in. ID silicone tube (see Figure 1a). This fit over the 3/16 inch Tygon, and when doubled over, tightly fit the 0.25 in. sample line. Quick disconnect type fitting can also be employed, and when the quick connects have a JG (John Guest) type push in connection to accept 0.25 in. LDPE sample tube, assembling the apparatus is efficient.

Alternative and easier connections can be made using 3/16 inch ID silicone tube. This is flexible, easy to cut, makes a tight, secure connection between 0.25 inch sample lines, the Fumiscope, the 3-way valve, and with the glass or Hammond Drierite tube. This set-up is shown in Figure 1b.

Tests with glass "Fumiscope" tubes. A series of tests was conducted using only the traditional glass desiccant tubes. The Fumiscope was zeroed, and then connected to a gas bag containg the supply of MeBr. The instrument was allowed to receive MeBr for 10 minutes. During this time, periodic readings and times were recorded, as the time in manures/seconds at which a stable inter reading was achieved. After 10 minutes, the gas flow was disconnected, allowing the Fumiscope to come to zero with the original used Drierite still in place. After 10 additional minutes the test was stopped. Following this, the test was repeated, except that the Fumiscope was allowed to come to zero by diverting fresh air through fresh Drierite via a 3-way Swagelok valve. The complete process was replicated three times with each method of zeroing.

Re-Zero with Hammond Drierite tube. The second set of tests was conducted in exactly the same way as the first set with glass tubes, except that the Drierite tube used was the commercial disposable Hammond Drierite tube.

Ascarite effect on zero. A similar arrangement of the Fumiscope was devised so that the instrument could be supplied with sample air from two alternate sources to test the effect of Ascarite on zero. The arrangement is shown in Figure 1c. One air source was filtered through a Hammond tube, followed by an in-line glass "Fumiscope" tube containing 10g of 8-mesh Ascarite-II (Thomas Scientific, Swedesboro, NJ). The alternative source of air was filtered through only a single Hammond Drierite tube. Inclusion of a 3-way valve (Swagelok, Solon OH) allowed for near

instantaneous switching of the air source from one side to the other. The Fumiscope was allowed to warm up for about 1-h prior to these tests. The Fumiscope air flow was adjusted at all times to provide ca. 452-460 ml/min of sample air. At exactly 5-minute intervals, the air flow was changed to the alternate side. This was repeated over 35 continuous. If the Fumiscope fluctuated between 0 and 1, the result was charted as ±0.5 g/m3. If the result fluctuated between -0 and +0, the result was charted -0.2 g/m3, only to illustrate small deviations from zero. This tabular adjustment was also applied to the second Ascarite test, following.

Tests with Ascarite and 1.0% CO_2. For the second test with Ascarite, as 40-liter gas bag with a mixture of 1.0 % v/v CO_2 was prepared. The air flow was alternated by switching between 1.0% CO_2 supplied through a Hammond Tube/Ascarite tube (previously exposed to 1.0% CO_2 for 5 min.) and alternately through clean Drierite only by turning the 3-way valve at 5-minute intervals. The result was paired tests with or without CO_2 over 85 continuous minutes. This arrangement is shown in Figure 1c. The method caused the Ascarite to scrub the CO_2 during alternate 5-min. periods, so that the effect was that the same Ascarite scrubbed the CO_2 for a cumulative total of 45 min.

Tests with CO_2 and common Ascarite. A third Ascarite test was devised in which a preparation of ca. 80 g/m^3 MeBr and 1.0% CO_2 v/v was supplied to the Fumiscope through two alternated Hammond tubes (one used with gas mix, the other with fresh air) followed by a shared Ascarite tube positioned after the 3-way vale proximal to the Fumiscope (Figure 1d). The gas flow was first supplied through Drierite, zeroed through the used, and then supplied again but zeroed with fresh air and unused Drierite. This test considered that a small Drierite tube did not contribute significantly to zeroing times, as shown in previous tests, and that ambient (ca. 385 ppm, est. 0.44 g/m^3 on a Fumiscope) CO_2 would also be scrubbed by the common Ascarite.

Results.

Tests with glass "Fumiscope" tubes. Figure 2 shows the effect on re-zero time when the air source was supplied through the Drierite used to take fumigant readings compared with a fresh Drierite tube. In this case, the Drierite tubes were the small glass tubes supplied with the Fumiscopes. Because of the small volume, MeBr air was flushed quickly. Still, re-zero time was improved by about 1 minute, but much less if outlier from first replicate was considered. The slightly delayed time to re-zero with used Drierite was due mainly to the MeBr content of the tube purging, more than desorption of MeBr from Drierite surfaces since Drierite capacity was small. With a small tube, practical when humidity is very low, the benefit of clean air re-zeroing was not significant (Figure 3). Also, the response of the

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Fumiscope to actual gas concentrations was faster with the small tube, as less internal tube volume was added to the input system and less Drierite was available to sorb MeBr.

Re-Zero with Hammond Drierite tube. Figure 4 shows the effect of using the larger capacity Drierite tube during fumigation monitoring and re-zeroing. With a larger tube, the Fumiscope response to supplied MeBr was not as rapid compared with the small tube, due to a larger internal volume of the system and the longer time needed to purge fresh air. There was a large difference in time to re-zero when Drierite used to monitor the MeBr was used compared with fresh air diverted to the Fumiscope through a fresh Drierite tube. Re-zero readings of 0-1 were obtained in ca. 5 minutes, compared with ca. 2 minutes when fresh air and unused Drierite was used. Figure 5 directly compares the two methods of re-zeroing. With the first replicate where used Drierite was in line, a Fumiscope value of 1.0 was reached after 5:17 minutes. After 10:00 minutes the value was unchanged. Switching to fresh Drierite and air immediately resulted in the reading going to zero, and when air was switched back to the used Drierite, the Fumiscope again indicated 1.0, thus suggesting the effect of residual MeBr lingers. Switching to fresh Drierite to zero the Fumiscope results in significantly reduced to zeroing time, which can be important in taking sequential, timely readings.

Ascarite effect on zero. The chart in Figure 6 indicated that switching between Drierite/Ascarite and Drierite only slightly increased Fumiscope readings. At one time (15 minutes) switching to Ascarite in-line resulted in a jump to +2, but this I believe can be attributed to drift or a power fluctuation. After re-zeroing after 20 minutes, the Fumiscope did not repeat the increase between 20 to 35 minutes with two additional changes. This is discussed in the next paragraph.

Tests with Ascarite and 1.0% CO_2. Considering that the Fumiscope was always zeroed at a reading of "0", not "-0" there was a very small bias to read fractionally higher. The precision of the instrument is in integers, therefore differences of 1-g/m^3 or less during operation must not be considered as highly significant. Further, periodic drift can account for small changes of less than 1-g/m^3 over time. The data in Figure 7 again show that switching sources to include had a slight effect on the zero readings. Switching to Ascarite + CO_2 usually resulted in a change in Fumiscope readings from 0/1 to 0 or -0. At the 30-min mark the instrument read 1 g/m^3, but the next switch did not result in a change. This suggests the some internal drift had taken place. From 45 minutes through 85 minutes there was little change in Fumiscope readings, and the Fumiscope was not re-zeroed during this time.

An additional factor is the presence of ca. 385 ppm (0.0385% v/v) CO_2 naturally occurring in the atmosphere. It has been shown that the Fumiscope responds to CO_2, indicating about 11.5 g/m^3 as MeBr per 1% CO_2. Natural CO_2 at about 385 ppm should therefore contribute about 0.44 g/m^3 to the Fumiscope reading. It can be seen in Figure 7, that when supply air was switched from the

"Drierite/Ascarite side" to the Drierite only side, the Fumiscope readings slightly increased, likely due to absence of Ascarite to scrub CO_2, and the natural occurrence of 385 ppm CO_2.

During these tests of Figure 7, the Fumiscope was initially zeroed with Ascarite in the sample stream, to read as 0, not to -0. Therefore the readings were slightly biased upwards by a fraction. It is also important to note that zeroing to zero may actually be between >-0 and <0.5 g/m3, thus supplying additional upward bias due to upward rounding by the instrument. When supplying zero air to speed re-zeroing of the Fumiscope, these results suggest it may not be essential to use Ascarite, even though Ascarite is used in the sample source monitoring the fumigant concentration. This would depend on the level of precision we wish to accept.

Tests with CO_2 and common Ascarite. Data of Figures 8-9 show the effect of a shared Ascarite tube as set up in Figure 1d. It has been previously shown that Ascarite has little effect on zeroing if the effect of scrubbing natural ambient CO_2 is discounted. Ascarite exposed to CO_2 compared with unused Ascarite did not affect zero response. Therefore, a common, shared Ascarite tube can make the zero process less complicated, avoiding the need for dual Ascarite tubes. The only effect of an Ascarite tube is to very slightly delay purging, as the volume of a glass Ascarite tube is small relative to the total system.

Discussion.

As with all of these tests, one must realize that the Fumiscope reads in 1.0 g/m^3 increments, so the initial zero process, and subsequent readings must be considered equal if differences are 0-1 g. Further, the air flow rate can be variable and adjusted, but it was impossible to duplicate exactly due to the coarseness of the flow adjustment. Additional error in time is introduced due to fluctuations in air density due to ambient pressure and temperature, though in this case the effects were minimal. In operational use, these factors would not be readily ascertained or consistent, except that response and zero times could vary.

The benefits of using fresh Drierite to re-zero the Fumiscope is less apparent, but measurable when the small glass (10 g, 8-mesh Drierite) tubes are used. The time advantage was only about one minute. However, the large tube with the finer mesh, larger capacity and polycarbonate/polyethylene construction (therefore more sorptive) illustrated a much greater benefit of using fresh Drierite to re-zero. The benefit of less time required to zero is measurable. But, the greater benefit is the reduced risk of entering a false base-line zero value if the process is carried out too soon. The need to wait two minutes, as opposed to over five minutes, allows readings to be taken in a more timely way, when three or more sequential readings are required. Even with this advantage, as mentioned above, residual MeBr of about 1 g/m^3 may have remained in the system after several more minutes. The main issue with re-zeroing with used Drierite is that residual MeBr remained and desorbed for some time in the Drierite/tube system, here more than 10 minutes, when supply was reconnected.

The Fumiscope should never be operated without Drierite between readings, as previous tests indicated that it affects zero for several minutes.

The necessity of using Ascarite where CO_2 is evolved is a policy matter. Ascarite will not significantly affect the Fumiscope zero while in proper use (not allowed to get plugged) and a shared Ascarite tube can be used proximal to any other arrangement of Drierite. This eliminates the small response to ambient CO_2, but will only slightly increase zero time. The advantage of using Ascarite is greater than a slight improvement in zero time.

The following recommendations are the result of the above tests.

1. If humidity is low, and a large Drierite is not required, zeroing through fresh Drierite does not give a significant time advantage and is not necessary. Response to actual MeBr is faster.
2. If larger capacity Hammond #26930 disposable Drierite tubes are used, switching to a fresh Drierite tube will significantly reduce zeroing times and reduce likelihood of prematurely setting a false zero baseline. Response to actual MeBr is slower.
3. Presence or absence of Ascarite marginally affected the zeroing process, though ambient, natural CO_2 may add up to $1/g/m^3$ to readings. Ascarite exposed to cumulative CO_2 did not significantly affect zero process.
4. Because of 3, above, a common shared Ascarite tube will mitigate the effect of natural CO_2, while not significantly affecting overall zero time.
5. Pictured Fumiscope setups are to be recommended.

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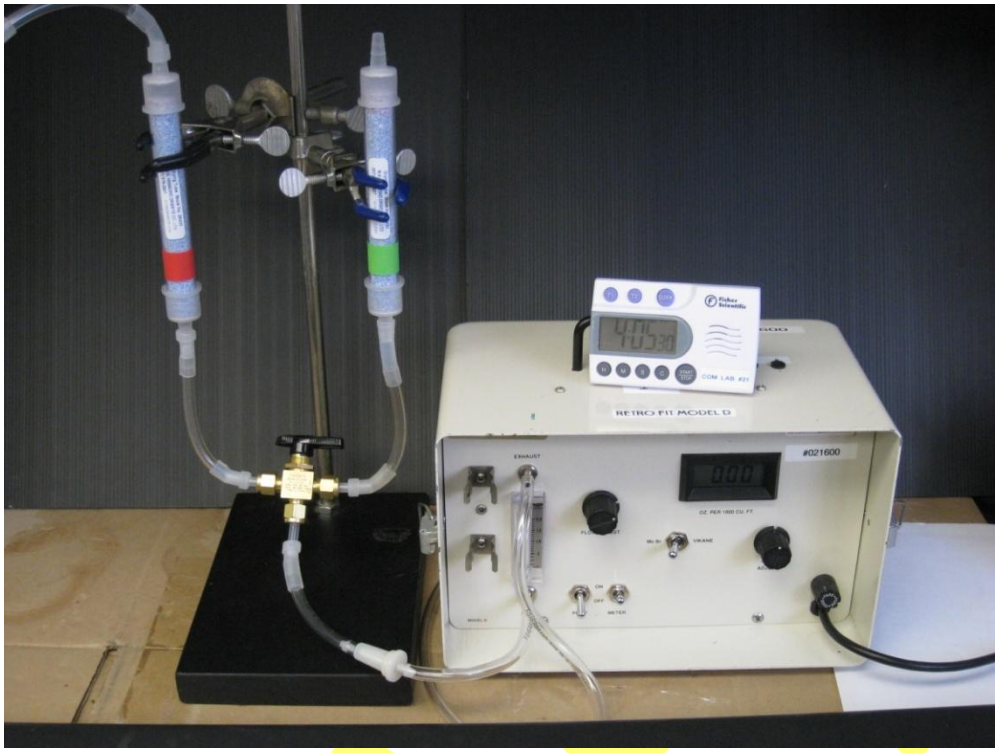


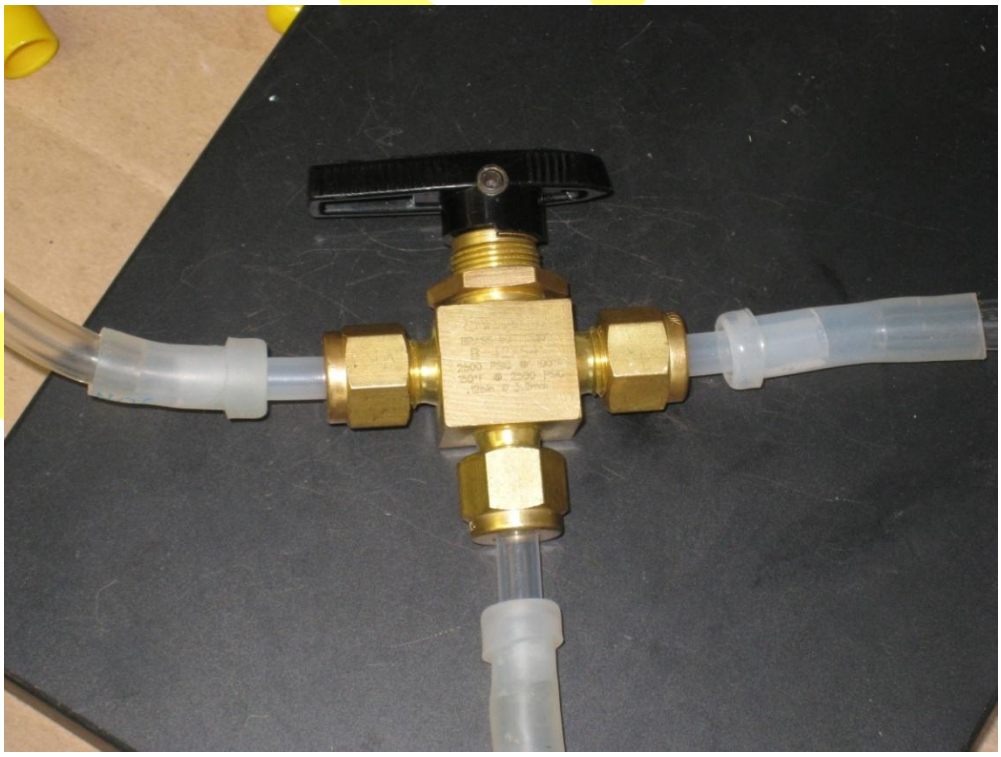
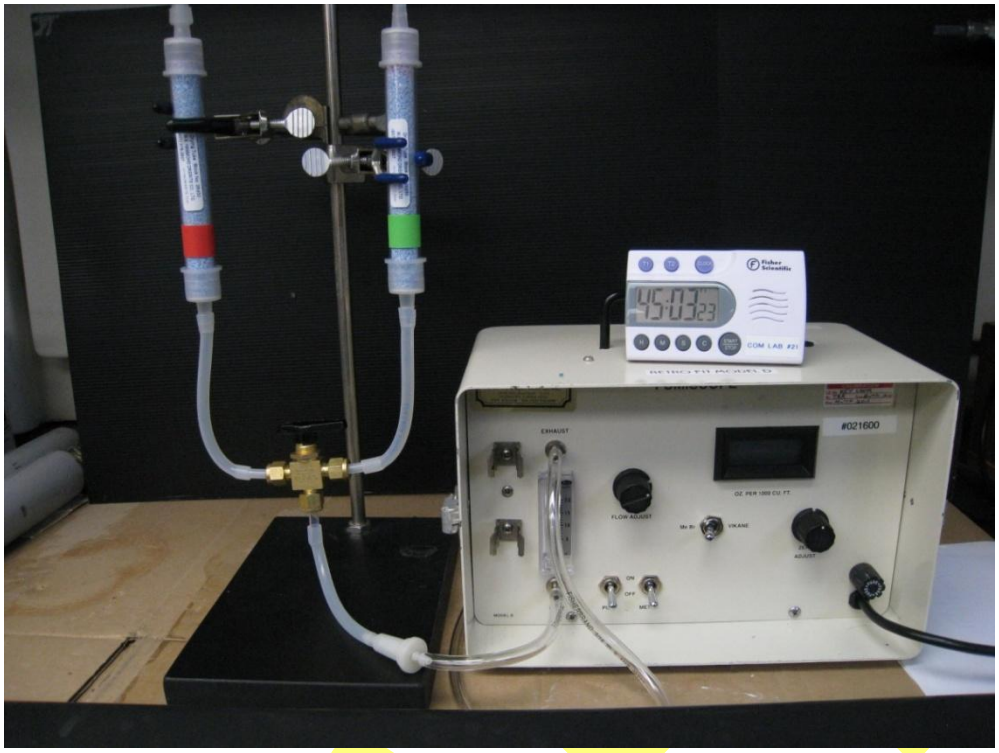


Figure 1a. Upper, Fumiscope with Swagelok B-43XS4 3-way valve to divert zero air from used Drierite to fresh Drierite tube. Lower, brass 3-way Swagelok valve with 0.25 in compression fittings. Also available with 1/8" female NPT thread and male thread brass hose barb push-on tube connections, purchased separately. In-line filter is optional.



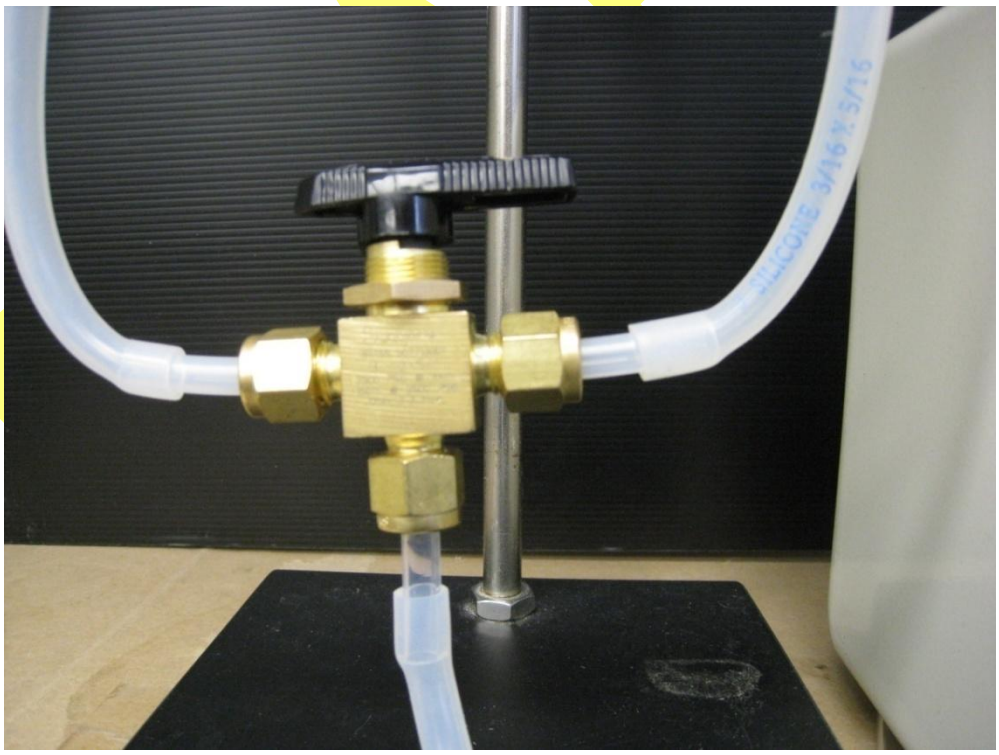


Figure 1b. Upper, Fumiscope with Swagelok B-43XS4 3-way valve to divert zero air from used Drierite to fresh Drierite tube. Lower, brass 3-way Swagelok valve with 0.25 in compression fittings. Secure connections were made with silicone 3/16 inch ID tube, which is easily cut and very flexible.

Figure 1c. Upper, experimental set-up to test effect of Ascarite on zero process by supplying alternate sources of sample air to a Fumiscope, via a 3-way precision valve. The first supply was filtered through Drierite plus 10 g Ascarite, and the second source was filtered through only Drierite. Lower, during these tests, two types of particle filters were used. However, additional testing had shown there was no difference between filter types on zero speed or end point. Picture is approximately actual size.

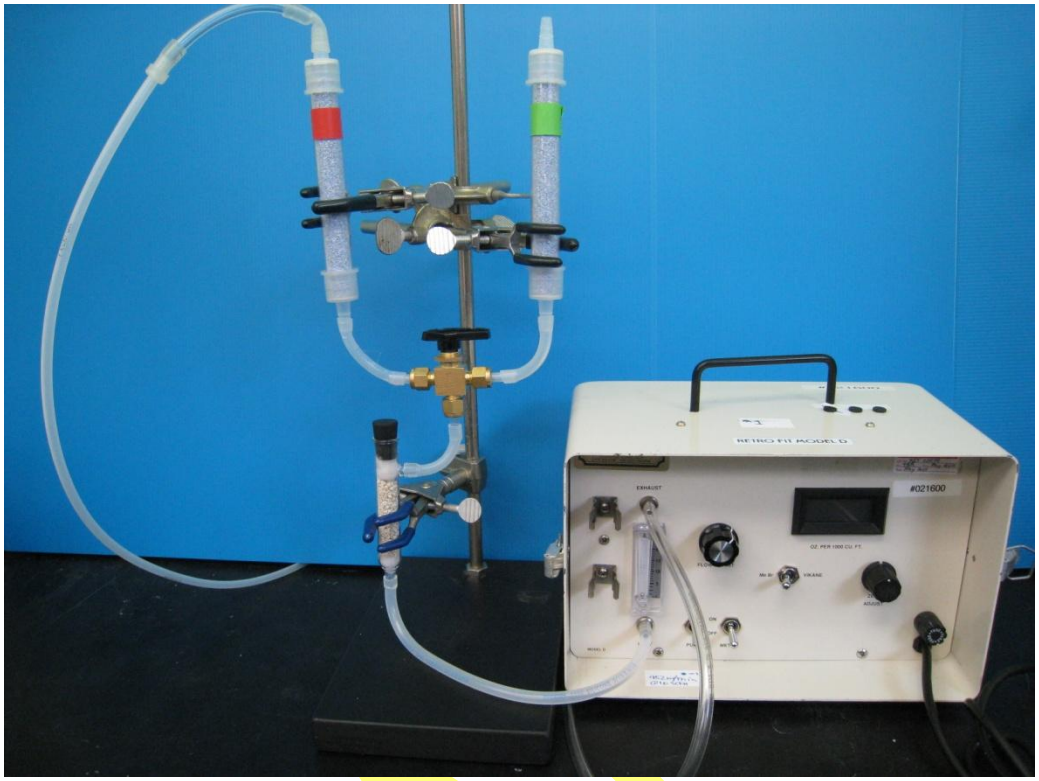
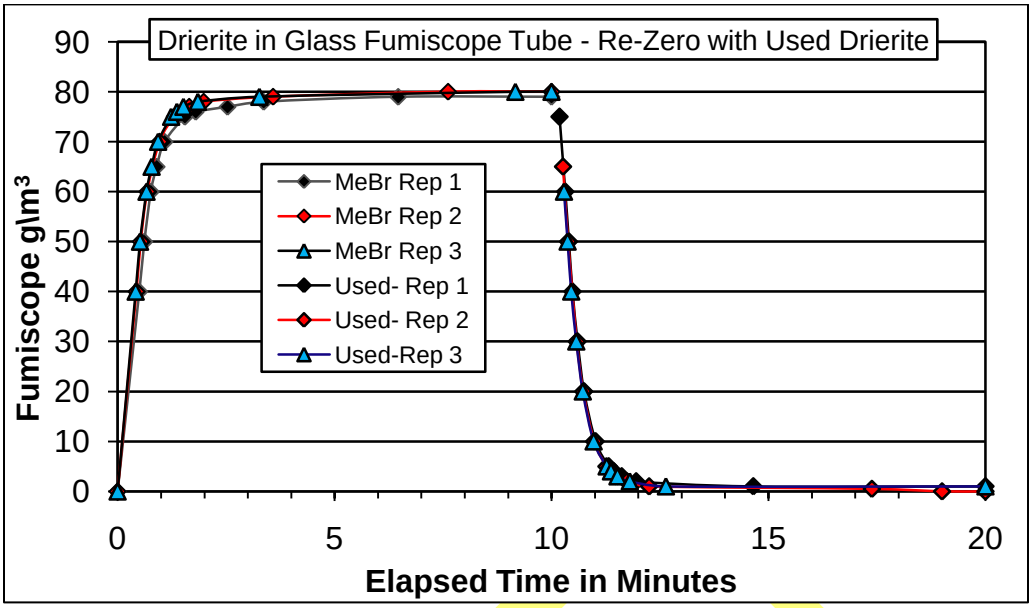


Figure 1d. Upper, Fumiscope with Swagelok B-43XS4 3-way valve to divert zero air from used Drierite to fresh Drierite tube with common Ascarite-II tube. Lower, brass 3-way Swagelok valve, with post-Drierite, shared glass tube containing 10 g of 8-10 mesh Ascarite-II.



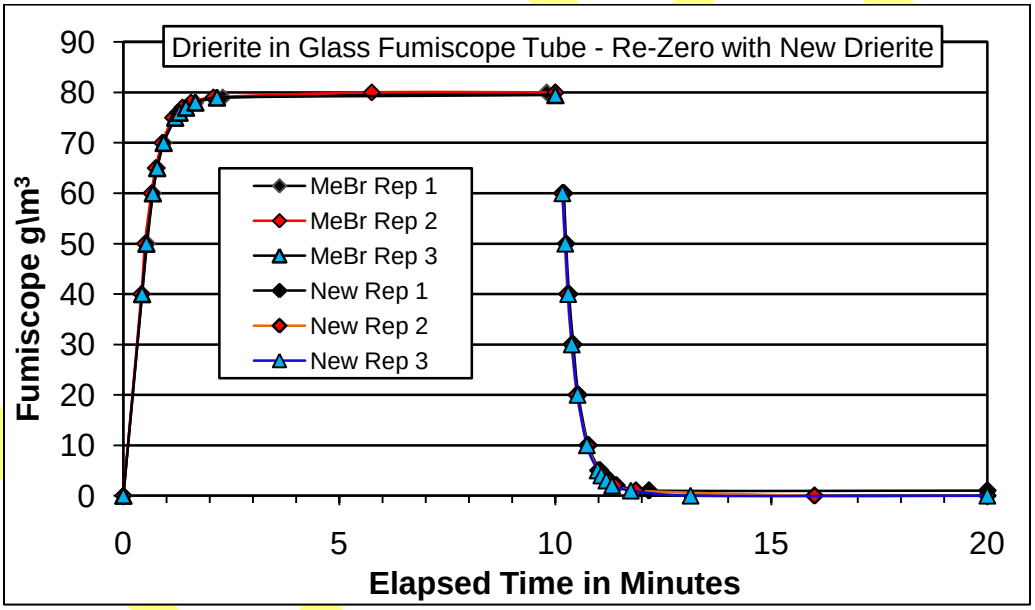
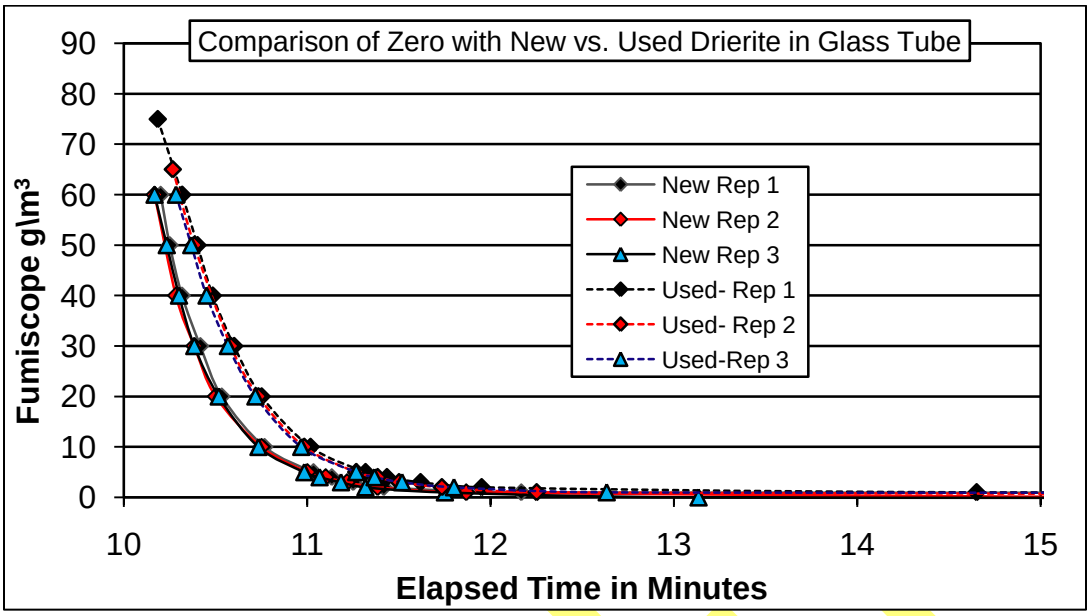


Figure 2. Response of the Fumiscope over 10- minutes to MeBr conditioned by passing through glass Drierite tubes (ca. 10 g) traditionally supplied with versions of the Fumiscope. The instrument was then re-zeroed for 10 minutes either by disconnecting the gas source (top) or a by resupplying MeBr and then re-zeroing through fresh Drierite by use of a 3-way valve (bottom). The test was replicated three times for each method. Fumiscope readings of 0-1 was achieved about one minute faster (ca. 1.5 vs. 2.5 minutes) using fresh Drierite, after supplying fresh Drierite.



ANOVA: Single Factor

SUMMARY

Groups	*Count*	*Sum*	*Average*	*Variance*
Used	3	9.53	3.176667	1.664133
New	3	5.79	1.93	0.0468

ANOVA

Source of Variation	*SS*	*df*	*MS*	*F*	*P-value*	*F crit*
Between Groups	2.3313	1	2.3313	2.7251	0.1741	7.7086
Within Groups	3.4219	4	0.8555			
Total	5.7531	5				

Figure 3. Upper. Direct comparison of zeroing speed of used vs. fresh Drierite in glass Fumiscope tubes. Lower. ANOVA. There was no significant difference in time required to zero to 1.0 on the Fumiscope. Perceived difference was due to residual MeBr in used tube, which was quickly purged.

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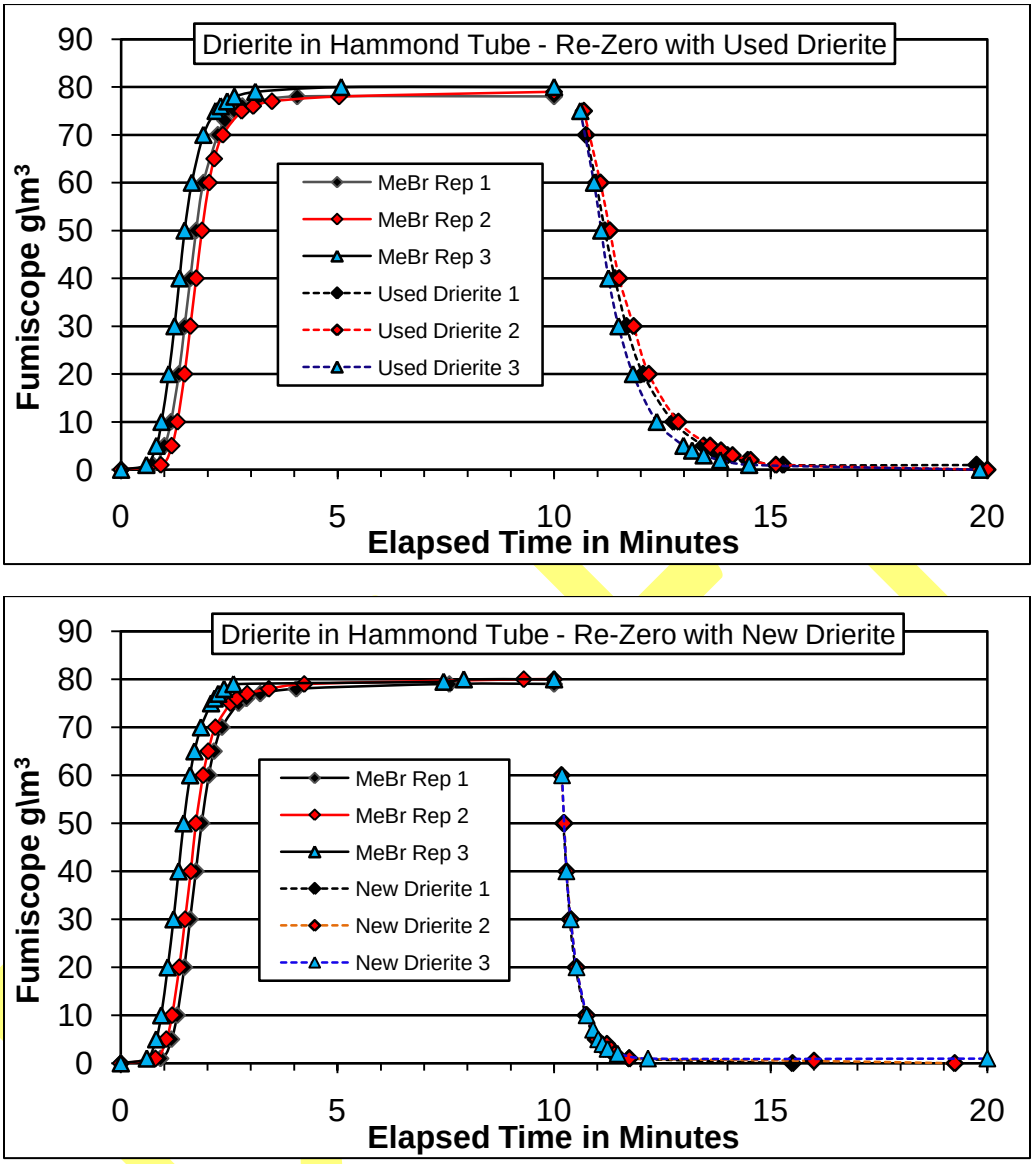
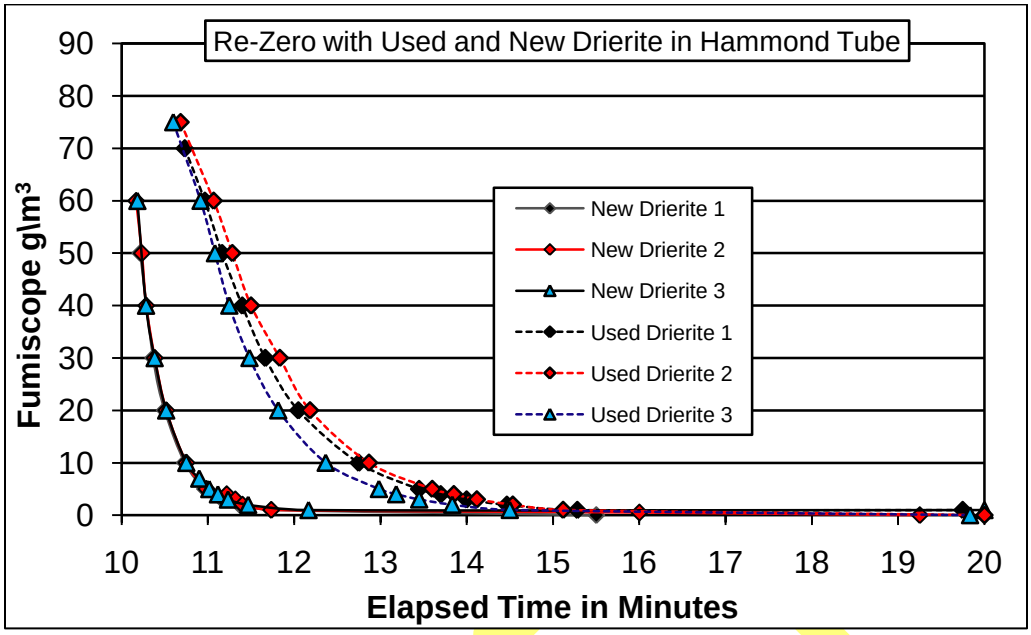


Figure 4. Response of the Fumiscope over 10- minutes to MeBr conditioned by passing through Hammond Drierite Company desiccant tubes (ca. 30 g) used with versions of the Fumiscope not supplied with traditional small glass tubes (Figure 1a, b). The instrument was then re-zeroed for 10 minutes either by disconnecting the only the gas source (top chart) or a by resupplying MeBr and then re-zeroing through fresh Drierite by diverting fresh air through a 3-way valve (bottom chart). The test was replicated three times for each method.



Anova: Single Factor

SUMMARY

Groups	*Count*	*Sum*	*Average*	*Variance*
Used	3	15.23	5.0766667	0.052033
New	3	5.63	1.8766667	0.064533

ANOVA

Source of Variation	*SS*	*df*	*MS*	*F*	*P-value*	*F crit*
Between Groups	15.36	1	15.3600	263.5402	0.0001	7.7086
Within Groups	0.2331	4	0.0583			
Total	15.5931	5				

Figure 5. Direct comparison of re-zeroing performance after 10 min of 80 g/m^3 exposure, by using the used Drierite or by diverting fresh air through unused Drierite to the Fumiscope by use of a 3-way valve. Re-zeroing by diverting fresh air through fresh Drierite resulted in a significant improvement in zeroing speed (ca. 2 minutes vs. 4.5-5.0 minutes) thus reducing the possibility of premature zeroing and creating a false baseline level. Improved time to reach 1.0 on Fumiscope was highly significant as determined by ANOVA.

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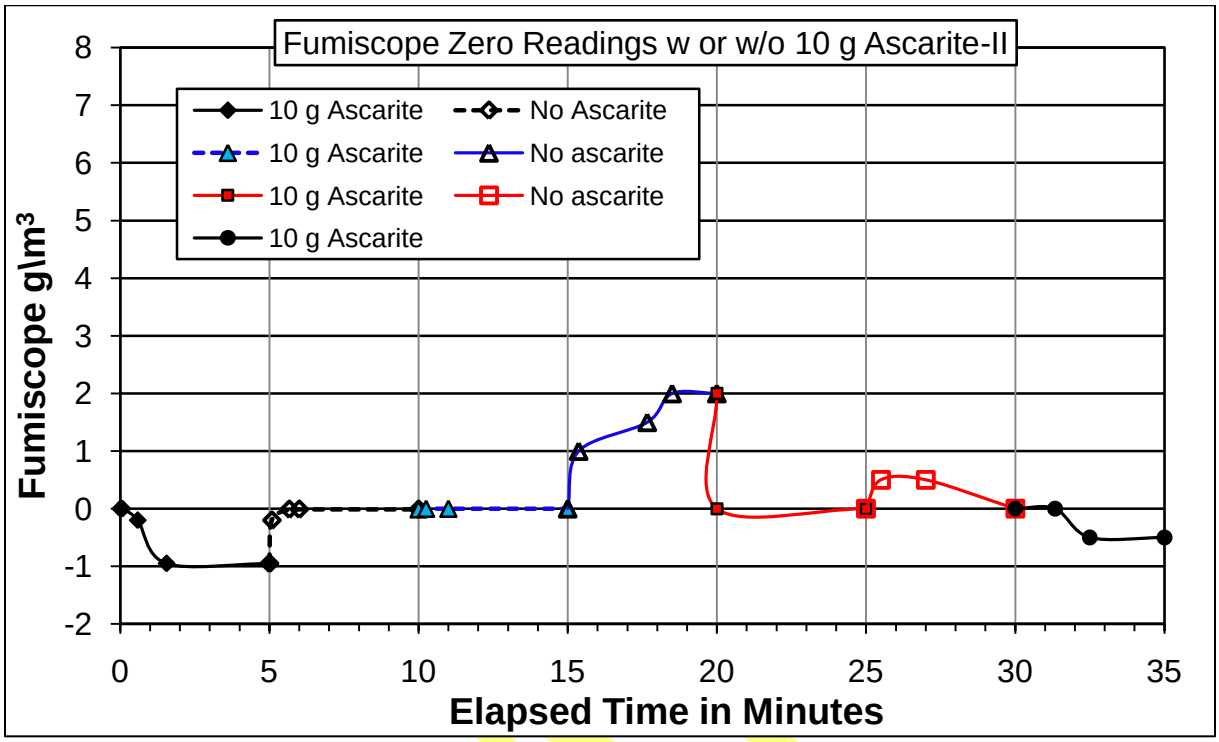

Figure 6. Fumiscope readings during which clean ambient air was supplied to the Fumiscope after passing through a Hammond Drierite tube + 10 g Ascarite in glass tube or alternately a Hammond Drierite tube only. Air sources were alternated at precisely 5 min. intervals.

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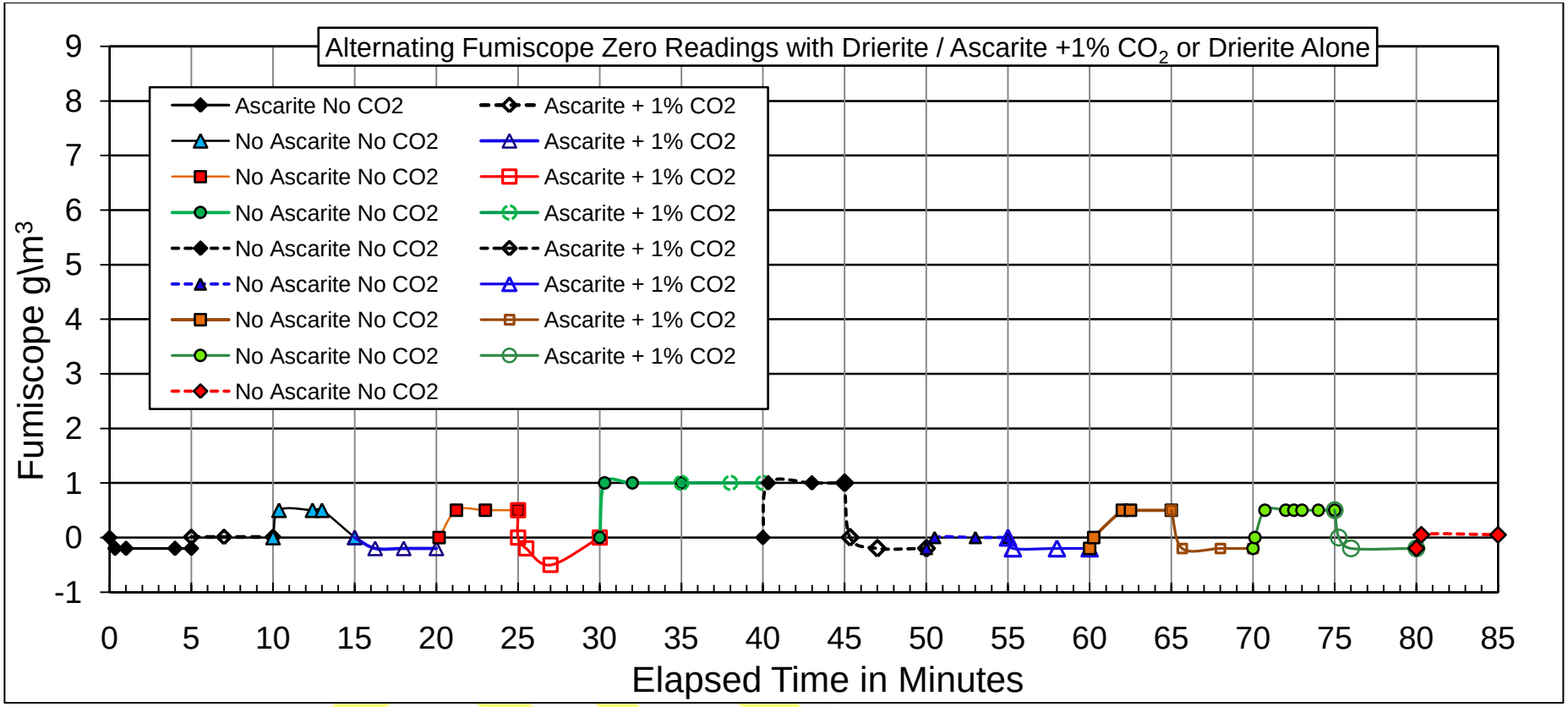
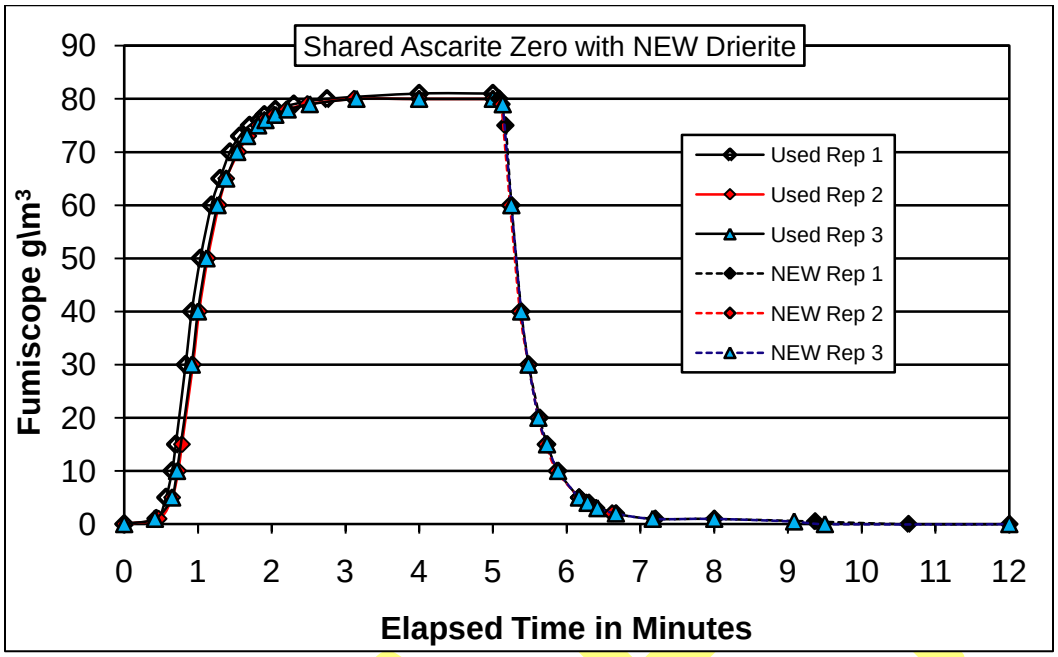


Figure 7. Fumiscope readings during which either clean ambient air or 1.0% v/v CO_2 was supplied to the Fumiscope after passing through a Hammond Drierite tube only or a Hammond Drierite tube + 10 g Ascarite in glass tube. Air sources were alternated at precisely 5 min. intervals, over 85 continuous minutes. Ambient CO_2 in the absence of Ascarite slightly increased the Fumiscope reading.



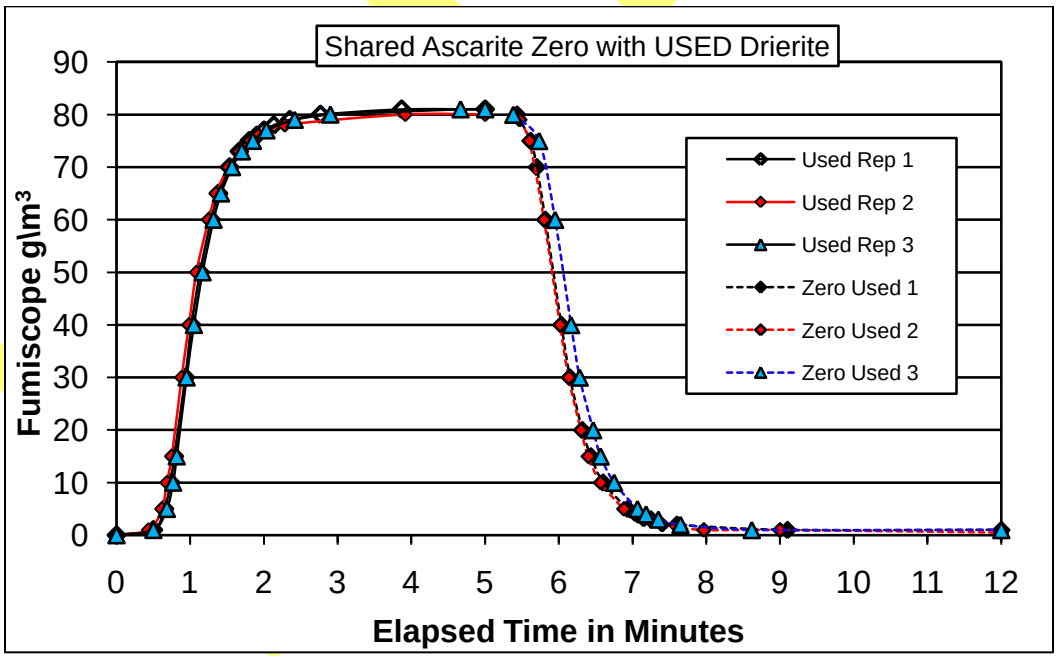
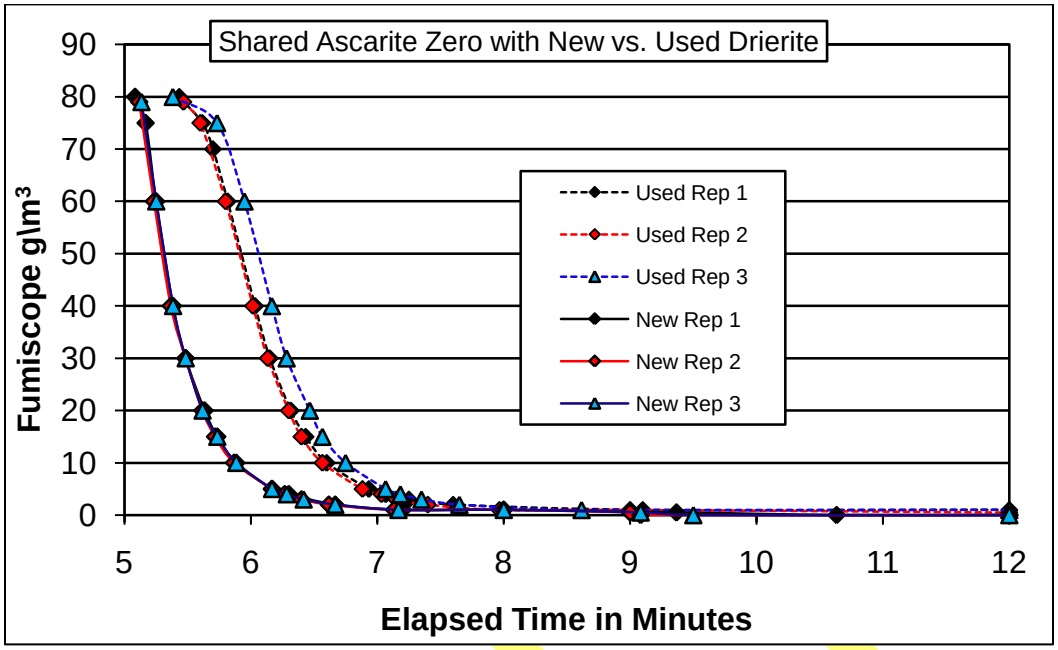


Figure 8. Fumiscope readings during which the zero was achieved through either a used Hammond tube exposed to 80 g/m^3 MeBr, or through a clean Hammond tube. Sources were alternated with a 3-way valve. Both sources were then passed through a common, shared Ascarite tube exposed to MeBr and 1.0% CO^2. The process was replicated three times. Therefore, the Ascarite was exposed to the CO_2 for a cumulative 15 minutes.



Anova: Single Factor — Time to Zero to 1 on Fumiscope

SUMMARY

Groups	*Count*	*Sum*	*Average*	*Variance*
Used	3	10.69	3.5633	0.3216
New	3	6.5	2.1667	0.0012

ANOVA

Source of Variation	*SS*	*df*	*MS*	*F*	*P-value*	*F crit*
Between Groups	2.9260	1	2.9260	18.1252	0.0131	7.7086
Within Groups	0.6457	4	0.1614			
Total	3.5718	5				

Figure 9. Above, direct comparison of the time to zero a Fumiscope through Drierite contaminated with 80 g/m^3 MeBr +1.0% CO_2 or alternately through unused Hammond tube only. Both gas sources shared a common Ascarite tube positioned proximal to the Fumiscope, after the 3-way valve. Three paired replicates were conducted. Lower, ANOVA of measured time for Fumiscope to reach a reading of 1.0 g/m^3.

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